

994 Longfield Avenue Louisville, Kentucky 40215 502/361-8447 FAX 502/361-4793

December 22, 2021

Ms. Laura Barlow LDG Development, LLC 1469 S. 4th St. Louisville, KY 40208

SUBJECT: GEOTECHNICAL REPORT

RESIDENTIAL DEVELOPMENT 8300 COOPER CHAPEL ROAD LOUISVILLE, KENTUCKY

GREENBAUM PROJECT NUMBER 21-273G

Dear Ms. Barlow:

Attached is the report of the geotechnical investigation that we carried out for the above referenced multi-family residential development. Soils at this site are competent to support spread footings designed based on an allowable net bearing capacity of up to 3,000 pounds per square foot. Bedrock is relatively shallow across the site and fat clay frequently overlies the bedrock. Further detail on foundations and other geotechnical considerations are provided in the body of the attached report.

If you have any questions regarding this report, please call.

Sincerely,

GREENBAUM ASSOCIATES, INC.

Sandor R. Greenbaum Sandor R. Greenbaum, P.E.

Principal Engineer

RECEIVED

JAN 2 4 2022

PLANNING & DESIGN SERVICES

21-MSUB-0024

GEOTECHNICAL INVESTIGATION

FOR

RESIDENTIAL DEVELOPMENT
8300 COOPER CHAPEL ROAD
LOUISVILLE, KENTUCKY

FOR

LDG DEVELOPMENT LLC 1469 SOUTH 4TH STREET LOUISVILLE, KY 40208

BY

GREENBAUM ASSOCIATES, INC.
994 LONGFIELD AVENUE
LOUISVILLE, KENTUCKY 40215

DECEMBER 22, 2021





© 2021, GREENBAUM ASSOCIATES, INC.

RECEIVED

JAN 24 2022

PLANNING & DESIGN SERVICES

21-MSUB-0024

Table of Contents

1.0	Introd	uction
2.0	Gener	al Geology
3.0	Invest	igation
4.0	Findin	gs
	4.1	Boring Results
	4.2	Laboratory Results
	4.3	Seismicity
5.0	Recon	nmendations
	5.1	Foundations
	5.2	Slab-on-Grade
	5.3	Site Preparation and Earthwork
	5.4	Dealing with Karst
	5.5	Earth Pressures
	5.6	Light- and Heavy-Duty Pavement
	5.7	Temporary Earth Slopes or Cuts

Limitations

APPENDIX

Site Location Plan (1 sheet)

Boring Location Plan (1 sheet)

Site Geology (1 sheet)

5.8

Soil Description Terminology/Rock Quality Determination (1 sheet)

Test Boring Reports (27 sheets)

Classification of Soils for Engineering Reports (1 sheet)

Grain Size Distribution (1 sheet)

Atterberg Limits Test (1 sheet)

1.0 Introduction

LDG Development intends build a residential development to be located at 8300 Cooper Chapel Road in Louisville, Kentucky. The proposed development is for multi-family buildings at the center of the development surrounded by single-family residences. A boring location plan is included in the appendix of this report that shows the approximate locations of the borings and the proposed development. A site location plan is also included in the appendix of this report.

Most of the site is covered by tall weeds with much of the western portion covered by woods. Elevation varies from about 670 in the southeast portion of the site to below 580 at the stream that passes north to south across the western portion of the site. A number of karst features are present to the east of the stream, over the western portion of the site.

We were contracted by LDG Development to carry out a geotechnical investigation directed at determining the foundation support characteristics of the materials upon which these buildings and associated pavement will be supported. Work was coordinated through Ms. Laura Barlow of LDG Development.

2.0 General Geology

Soils at this site are shown by the Kentucky Geological Survey to be residuum, the residual product of weathering of the local bedrock. Bedrock is shown to be the Louisville Limestone over the bulk of the site with the underlying Waldron Shale and Laurel Dolomite exposed along the stream on the west side of the site (see included drawing of Site Geology). The Geological Survey describes the Louisville Limestone as:

Dolomitic limestone and dolomite, yellowish-gray, light-olive-gray, pale yellowish brown to very pale orange, very fine grained, argillaceous in part; stylolitic, very thin to thin bedded in upper part, very thick bedded near base; irregular rubbly bedding common, typified in exposures along Kentucky Turnpike; locally shaly in 10 foot zone about 20 feet above base; contains calcite filled pockets and thin veinlets of calcite; chert rare in lower beds but common in discontinuous 0.2 foot thick layers in uppermost few feet. Unit reportedly thickest in vicinity of abandoned quarry 1-mile due east of Hubers Kenlite Station. Supports broad westward dipping surface east of Kentucky Turnpike; outcrop areas locally marked by narrow, steep walled

solution cavities and small sinks; some beds form continuous persistent ledges rimming steep walled stream valleys. One such ledge top approximately 40 feet above the base, another at about 60 feet above the base. Dolornitized fossils common as casts are abundant in some layers; include brachiopods, horn corals, colonial corals, chain corals, and algal mat remains. Basal contact with underlying shale distinct to gradational over as much as 2 feet.

The Geological Survey describes the Waldron Shale as:

Shale, medium gray, olive gray, and greenish gray to medium bluish gray, weathers yellowish gray; dolomitic, pyritic; near base of quarry exposure at north border of quadrangle unit contains dolomitized brachiopods, small crinoid stems, trilobite fragments, and dark to brownish gray organic discs less than 1 mm in diameter that resemble the palynomorph Tasmanites. Weathers in gentle slopes, locally forms bench; contact probably conformable. Soils on unit belong mainly to Beasley Series.

The Geological Survey describes the Laurel Dolomite as:

Dolomite and minor shale in three distinct parts: Uppermost part is dolomite, light olive gray to olive gray with dark gray mottling, weathers yellowish gray to grayish orange; finely crystalline to medium crystalline (0.02 to 0.25 mm); distinguished by even "quarry stone" bedding ranging in thickness from 0.2 to 2.8 feet; locally contains interbedded and intermixed oolitic dolomite in upper 1.5 feet; some beds contain styolites. Bedding planes commonly accentuated by thin shale partings; burrows common. Middle part is moderate brown and medium gray to medium light gray dolomite that weathers yellowish gray to pale yellowish orange; mottled, vuggy, without distinct partings; calcitic; contains dolornitized brachiopods. cephalopods, trilobites; planar bedded finely crystalline limestone (calcilutite) near base. Middle and basal parts of unit form massive ledges marked by honeycombed surface. Basal part, in descending order, is shale, dolomite, and shaly dolomite. Shale is dark greenish gray, weathers grayish yellow; dolomitic, calcareous; in a single bed 1.5 to 2.5 feet thick. Dolomite and shaly dolomite are greenish gray to light olive gray, weather same to grayish orange; finely crystalline to medium crystalline (0.02 to 0.25 mm); beds 0.3 to 2.0 feet thick. Basal contact gradational through as much as 3 feet with dolomitic shale and shaly dolomite of underlying formation; contact commonly coincides with break in slope. Soils developed on formation commonly include Russellville, Dickson, and Crider Series. Thickness of residuum generally ranges from 5 to 12 feet on uplands.

3.0 Investigation

Twenty-seven borings were carried out across the site by standard penetration procedures to refusal on bedrock. A Diedrich D-25 track-mounted drill rig was used to carry out the borings through the use of 3 ¼-inch inside diameter hollow stem augers and an automatic hammer. The boring locations were staked using a nylon tape from existing topography, so boring locations are only as accurate at this method allows.

The standard penetration procedure involves driving a standard 2-inch diameter split spoon in the formation at selected intervals using a 140-pound hammer falling through 30 inches. The blow counts for each 6 inches of drive, to a total of 18 inches, are recorded and the number of blows for the 12 inches after the first 6 inches is a standard measure of the condition of the soil. As the split spoon is removed from the ground, it retrieves a sample of the soil in a disturbed condition. Nevertheless, this sample is suitable for certain classification tests and is representative of the soils at the depth tested.

Soil samples were returned to the laboratory where a program of testing was carried out. This testing included a grain size analysis, an Atterberg Limits' test and a natural moisture determination.

Grain size determination arrives at a curve of grain size against that fraction of the soil that is finer than that particular grain size. It also allows the determination of the clay fraction, silt fraction, sand fraction, etc. in any particular soil sample. Based on this division of grain sizes, the field soils classifications are refined and the boring logs adjusted. In the case of fine-grained soils, the soils are largely silt and clay; thus requiring that the soils be suspended in an aqueous medium and the rate at which the particles drop out is measured in order to arrive at the grain size distribution. Silt and clay grains are so fine that sieve analysis alone will not function in this range. The coarse fraction of this sample is separated from the fine and run through a nest of sieves in order to further detail the grain size distribution in the coarse range. In this case only the sieve analysis portion of the test was performed since little sand and silt was present in the soil samples selected for testing.

The Atterberg Limits' determination arrives at those moisture contents at which the soil turns from a solid state to a plastic condition (the Plastic Limit) and then from a plastic condition to a liquid condition (The Liquid Limit). The points in question are arrived at by standard procedures that accept specific cohesive and flow properties of the soil as standards for these limits. Knowing the moisture content of the soil in relation to these limits provides a broad measure of the soil

strength and soil characteristics. The arithmetic difference between these two limits is called the Plasticity Index and all three together are used for classifying the soils in a number of standard systems.

The natural moisture determination arrives at the in-situ moisture content of the soil and is useful for correlating the strength of various samples of like texture and in conjunction with the Atterberg limits, gives a strong measure of the strength range the soils are likely to be found in.

4.0 Findings

4.1 Boring Results

This site is generally covered by about 5- to 6-inches of topsoil. Below this, soil is moist, stiff, brown or brown and gray mottled, lean clay or moist, medium dense, brown, silt. Soils near the bedrock are frequently moist, stiff to very stiff, tan, fat clay. Since bedrock is shallow, fat clay can sometimes be quite shallow as well. Auger refusal was encountered between 1.0- and 8.3-feet depth. Groundwater was not encountered in any borings but may be present seasonally.

The tables below and continued on at the top of the following page provide a tabulation of N-values as measured by the standard penetration test, corrected for the energy of the automatic hammer, along with depth to auger refusal.

Depth	B-01	B-02	B-03	B-04	B-05	B-06	B-07	B-08	B-09
1 – 2.5 feet	12	50/3"	23	20	12	12	12	10	13
3.5 – 5 feet	12		25	20	18	50/3"	14	10	
6 – 7.5 feet	21			50/4"	50/3"			50/0"	
Auger Refusal	7.7'	1.6'	5.5'	6.3	6.3	4.5'	5.7'	6.01	4.4'

Depth	B-10	B-11	B-12	B-13	B-14	B-15	B-16	B-17	B-18
1 – 2.5 feet	14	14	10	13	10	8	13	8	10
3.5 – 5 feet	16	20	17	17	12	50/0"	14		
6 – 7.5 feet		50/3"	13	50/1"	13				
Auger Refusal	6.0'	6.3'	8.3'	6.1'	8.3'	4.5'	5.8'	3.01	3.5'

Depth	B-19	B-20	B-21	B-22	B-23	B-24	B-25	B-26	B-27
1 – 2.5 feet		31	14	14	50/0"	50/3"	50/5"		50/2"
3.5 – 5 feet			17	21					
6 – 7.5 feet				26					
Auger Refusal	0.7'	3.0'	6.0'	7.6'	1.5'	3.9'	3.2'	1.0'	3.3'

4.2 Laboratory Results

A sample of soil from shallow depth was tested and classified and was found to be lean clay. The result of this testing is summarized in the table below with more detailed results provided in the appendix of this report. Moisture content is shown graphically on the boring logs.

	Grain	Size Distr	ibution	Atte	erberg Li	mits		oil fication
Soil Sample	Percent Sand	Percent Silt	Percent Clay	Liquid Limit	Plastic Limit	Plasticity Index	Unified	AASHTO
B-07 @ 1' – 2.5'	7	44	49	42	21	21	CL	A-7-6

4.3 Seismicity

By the 2018 edition of the Kentucky/2015 International Building Code, this is a Very Dense Soil and Soft Rock Profile, Site Class C. The Spectral Response Acceleration Coefficients, for this area, as provided by U.S.G.S., FEMA Design Parameters are:

$$S_{S} = 0.200 \ g \qquad \qquad S_{MS} = 0.240 \ g \qquad \qquad S_{DS} = 0.160 \ g$$

$$S_{1} = 0.105 \ g \qquad \qquad S_{M1} = 0.177 \ g \qquad \qquad S_{D1} = 0.118 \ g$$

5.0 Recommendations

5.1 Foundations

These buildings may be supported on spread footings bearing on shallow soil or structural fill placed in accordance with section 5.3 of this report. These foundations may be designed based on an allowable net bearing capacity of up to 3,000 pounds per square foot.

Rock is relatively shallow across the site, as shallow as 1- to 3-feet in several locations. Where rock is encountered in foundation bearing surfaces it should be removed to a depth at least one foot below the foundation bearing surface and refilled with lean clay or sand compacted to between 88 and 92 percent of the soils maximum dry density as measured by the Standard Proctor (ASTM D-698). This will act as a cushion that will transition from soil bearing foundations to foundations bearing near bedrock to limit distress in the building. Otherwise, cracks could develop in the building where foundations go from soil bearing to rock bearing due to a rapid change in settlement.

Once foundation bearing surfaces are exposed, an engineer or senior engineering technician from this office should be present to view all bearing surfaces to determine the presence of soft soils. Where soft areas are encountered, undercut will need to extend to firm material or to a level determined to be acceptable by the geotechnical engineer and should be refilled with either lean concrete (fc' = 2,000 psi) or open-graded stone such as Number 57 stone.

Soil bearing foundations exposed to weather must bear at least 30 inches below finished grade in order to insulate the bearing strata from freezing. Interior foundations protected from freezing are exempt from this requirement. Continuous footings must be at least 16 inches wide and isolated footings must be at least 24 inches wide.

Settlement of foundations designed based on the above criteria should be below that which is considered acceptable for this type of construction; that is total settlement should be less than one inch and differential settlement should be less than three quarters of an inch.

For shallow foundations, friction along the base of the footing can be used to resist lateral forces. A friction coefficient of 0.35 may be used, which assumes that the footing concrete is placed directly against the natural cut faces. The coefficient of friction value recommended is an ultimate value and a minimum factor of safety of 1.5 must be applied when determining the allowable sliding resistance.

5.2 Slab-On-Grade

Prior to placement of the fill in the slab area, the subgrade must be proofrolled and carefully examined by a geotechnical engineer for areas of soft or loose soil. If soft or loose soils are encountered, they must be undercut and refilled in accordance with instructions given by the geotechnical engineer's on-site representative. Undercut and refill in soft areas consists of excavating to a depth up to two feet below subgrade elevation and refill should be with "Surge Rock", 6-inch minus or Number 3 stone. Large rock should not be used in areas where trenching will be required to install piping or conduit.

Should fat clay be found to be in the subgrade of slab-on-grade, there are two means of preventing the problem of softening and swelling below the slab. These are:

- Lean clay should be used as fill in the top foot in fill areas and the top foot of soil in cut areas should be replaced with lean clay where fat clay is found to be present.
- The slab subgrade should be treated with 5 percent lime to at least 12 inches depth to modify the fat clay so that it is no longer subject to unacceptable volume change.

A slab-on-grade that is structurally separated from the walls, columns and foundations is preferable, though thickened slab may be used. Separation of slab-on-grade from foundations will minimize the stress caused by possible differential settlement between the slabs and the foundations and between adjacent slabs. A vapor barrier must be incorporated into the design and at least four inches of Dense Graded Aggregate (DGA) should underlie the slab. The floor slab may be designed based on a Modulus of Subgrade Reaction of 105 kips per cubic foot.

5.3 Site Preparation and Earthwork

Prior to fill placement all vegetation and topsoil (soil containing more than 4 percent organic content) must be removed from below the area to be filled. Where trees or bushes have been present, the entire rootball should be removed and the resulting excavation should be refilled with soil compacted as described in this section of the report. Then, prior to placement of fill, the exposed subgrade should be proofrolled by a fully loaded tri-axle truck to delineate any yielding or rutting areas that may require treatment such as undercut and refill or drying.

All fill should be placed in lifts not exceeding 8 inches in uncompacted thickness and must be compacted to at least 98 percent of the soils maximum dry density as determined by the Standard Proctor (ASTM D-698). Soil moisture content should be within 2 percent of optimum as determined from the Standard Proctor.

Soil from any off-site borrow sources should be tested and approved by this office prior to being used on the site. Satisfactory borrow materials are those falling in one of the following classifications: GC, SM, SC, ML, or CL. Soil types MH, CH and OH soils and peat are unsatisfactory borrow materials.

Fill should be placed in horizontal lifts where fill is to be placed on a slope, horizonal benches should be cut into the slope to allow placement of horizonal lifts of soil. Fill slopes must not exceed two horizontal to one vertical, preferably 2.5-or 3-horizontal to one vertical to allow for mowing of the slopes with common equipment.

The site should be maintained in a well-drained condition both during and after construction. Site grading should provide for drainage of surface run-off away from the proposed buildings and pavement.

The placement of compacted fill should be carried out by an experienced excavator with the proper materials. The excavator must be prepared to adapt his procedures, equipment and materials to the type of project, to weather conditions, and the structural requirements of the engineer. Methods and materials used in summer may not be applicable in winter; soil used in proposed fill may require wetting or drying for proper placement and compaction. Conditions may also vary during the course of a project or in different areas of this site. These needs should be addressed in the project drawings and specifications.

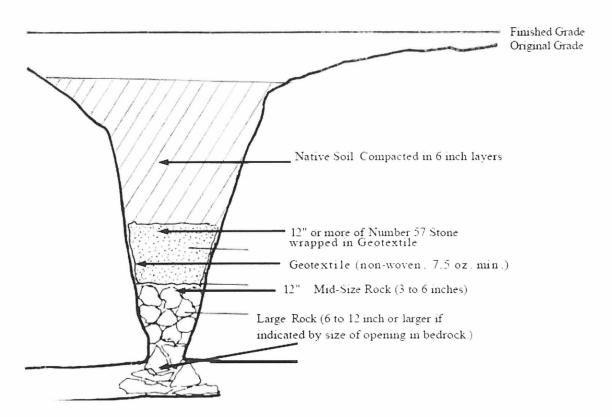
During freezing conditions, the fill must **not** be frozen when delivered to the site. It also must not be allowed to freeze during or after compaction. Since the ability to work the soil while keeping it from freezing depends in part on the soil type, the specifications should require the contractor to submit a sample of his proposed fill before construction starts, for laboratory testing. If the soil engineer determines that it is not suitable, it should be rejected. In general, silty sand, clayey sand, and cohesive/semi-cohesive soils should not be used as fill under freezing conditions. All frozen soil of any type should be rejected for use as compacted fill.

It is important that compacted fill be protected from freezing after it is placed. The excavator should be required to submit a plan for protecting the soil. The plan should include details on the type and amount of material (straw, blankets, extra loose fill, topsoil, etc.) proposed for use as frost protection. The need to protect the soil from freezing is ongoing throughout construction and applies both before and after concrete is placed, until backfilling for final frost protection is completed. Foundations placed on frozen soil can experience heaving and significant settlement, rotation, or other movement as the soil thaws. Such movement can also occur if the soil is allowed to freeze after the concrete is placed and then allowed to thaw. The higher the percentage of fines (clay and silt) in the fill, the more critical is the need for protection from freezing.

The contractor should be required to adjust the moisture content of the soil to within a narrow range near the optimum moisture content (as defined by the applicable Proctor or AASHTO Test). In general, fill should be placed within 2% of optimum moisture. The need for moisture control is more critical as the percentage of fines increases. Naturally occurring cohesive/semi-cohesive soil are often much wetter than the optimum. Placing and attempting to compact such soils to the specified density may be difficult. Even if compacted to the specified density, excessively wet soils may not be suitable as pavement subgrades due to pumping under applied load. This is especially true when wet cohesive/semi-cohesive soil is used as backfill in utility trenches and like situations. Excessively wet soil in thick fill sections may cause post-construction settlement beyond that estimated for fill placed at or near (±2%) the optimum moisture content.

5.4 Dealing with Karst

Several karst features are shown on the topographic survey of the site and were observed by a geotechnical engineer when boring locations were staked. If construction is to take place in the areas of these potential karst features are present, it will be necessary to expose the bedrock at these locations to determine if they are truly karst features or are due to another cause and, where karst features are present, install a filter in any crevices or openings in the bedrock. A diagram of a typical treatment of a karst feature using a filter is provided at the top of the following page. Treatment should be on a case-by-case basis under the guidance of a geotechnical engineer. We are available to assist you with the design of the filter at each of these locations. Such a filter will allow water to pass into the opening in the bedrock, but prevent erosion of soil, thus preventing subsidence at that location and making construction possible.



5.5 Earth Pressures

Any retaining walls should be constructed with a drainage blanket of sand or a synthetic drainage material. Synthetic drainage media should be available from suppliers of geotextile. The wall should be drained at its base by a perforated PVC underdrain or weepholes at a spacing of not more than 10 feet. Where a relatively thin drainage blanket is used, the retaining wall should be designed based on a coefficient of active earth pressure (K_a) of 0.36 and a soil unit weight (γ_w) of 130 pounds per cubic foot. This results in an equivalent fluid pressure of 47 pounds per cubic foot. Where granular backfill completely fills the area defined by a plane extending upward from the base of the wall at a 45-degree angle, the retaining wall may be designed based on a coefficient of active earth pressure (K_a) of 0.27 and a soil unit weight (γ_w) of 130 pounds per cubic foot. This results in an equivalent fluid pressure of 35 pounds per cubic foot.

However, where the wall is restrained from movement, as in the case of building basement walls bearing against the basement slab or building frame, the wall must be designed based on the "at rest" earth pressure. The coefficient of "at

rest" earth pressure (K_0) is 0.47 with a soil unit weight (γ_w) of 130 pounds per cubic foot in the case of a thin drainage blanket behind the wall, resulting in an equivalent fluid of 61 pounds per cubic foot unit weight. Where granular backfill completely fills the area defined by a plane extending upward from the base of the wall at a 45-degree angle, the retaining wall may be designed based on a coefficient of "at rest" earth pressure (K_0) of 0.43 and a soil unit weight (γ_w) of 130 pounds per cubic foot. This results in an equivalent fluid pressure of 56 pounds per cubic foot.

The table below summarizes the design earth pressures.

	Active Earth Pressure Coefficient (K _a)	Passive Earth Pressure Coefficient (K _P)	Coefficient of Earth Pressure at Rest (K ₀)	Equivalent Fluid Pressure on Cantilever Walls	Equivalent Fluid Pressure on Braced Walls
Fill Material/Local Soils	0.36	2.77	0.47	47 pcf	61 pcf
Granular Backfill	0.27	3.69	0.43	35 pcf	56 pcf

Surcharge above the wall will add additional load. A uniform surcharge must be multiplied by the appropriate coefficient of earth pressure to determine the additional load applied to the wall.

Any retaining wall design must use appropriate factors of safety. It is critical that drainage be provided as mentioned earlier in this section in order to avoid hydrostatic pressure. Hydrostatic pressure would increase pressure against the wall substantially.

5.6 Light- and Heavy-Duty Pavement

Pavement subgrade should be examined and proofrolled as described under "Floor Slabs". If soft areas are encountered, the soft soils will need to be undercut and refilled in accordance with the instructions of the geotechnical engineer's on-site representative. Subgrade stabilization was discussed in section 5.2 for slab-on-grade. The same approach should be taken for pavement subgrade, but the requirement for a stable, non-yielding subgrade is even more important in the case of asphalt pavement.

A pavement analysis was conducted using a life cycle of 20 years and a cumulative 18-kip equivalent single axle load of 20,000 for light traffic loads and 160,000 for moderate traffic loads. Recommendations are provided for both flexible and rigid pavement systems. However, rigid pavement should be used in special truck traffic areas, such as those areas which receive frequent traffic by garbage trucks. The concrete pavement should extend throughout the areas that require extensive turning and maneuvering of garbage trucks or other heavy trucks. Heavily loaded pavement areas that are not designed to accommodate these conditions often experience localized pavement failures, particularly if flexible pavement sections are used.

The minimum recommended thickness for both hot mixed asphalt concrete (HMAC) and reinforced Portland cement concrete (PCC) pavement sections are presented in the table at the top of the following page for the described light, moderate and special traffic condition.

	Recomme	ended Paver	nent Section	n	
	Li	ght	Mod	erate	Special
Component	Rigid	Flexible	Rigid	Flexible	Rigid
Reinforced Portland Cement Concrete (PCC)	5 inches		6 inches		7 inches
Hot Mixed Asphalt Concrete (HMAC)		3 inches		4 inches	
Crushed Limestone Base (Dense Graded Aggregate)	4 inches	8 inches	4 inches	8 inches	4 inches

The Portland cement concrete should be air-entrained and conform to ASTM C-94 (Standard Specifications for Ready-Mixed Concrete) and have a minimum compressive strength of 4,000 pounds per square inch. Reinforcing should meet the requirements of ACI.

Hot mix asphalt concrete and Dense Graded Aggregate should meet the requirements of the Kentucky Transportation Cabinet. The top inch and a half of asphalt should be a surface mix, the remainder being a base mix.

5.7 Temporary Earth Slopes or Cuts

Temporary earth cuts necessary to construct foundations or utility lines should be no deeper than 4 feet without benching or sloping. Cuts deeper than this should be sloped no steeper than one horizontal to one vertical or should have benches every 2 feet of height equating to this slope. If vertical faces deeper than

4 feet are used, bracing designed for short term loads may be used. Excavations should comply with OSHA regulations.

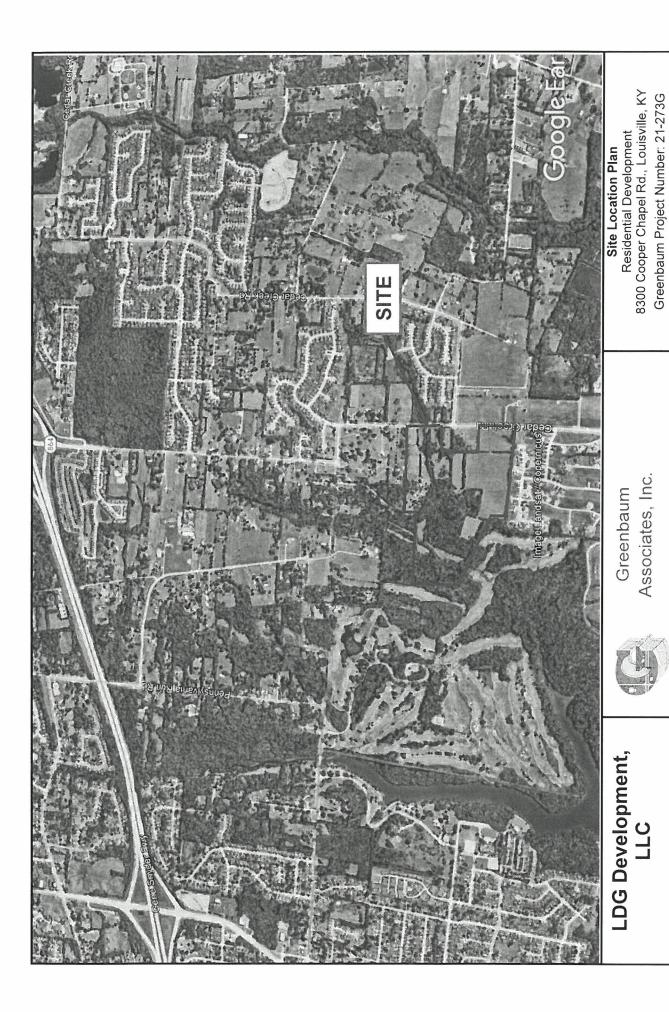
5.8 Limitations

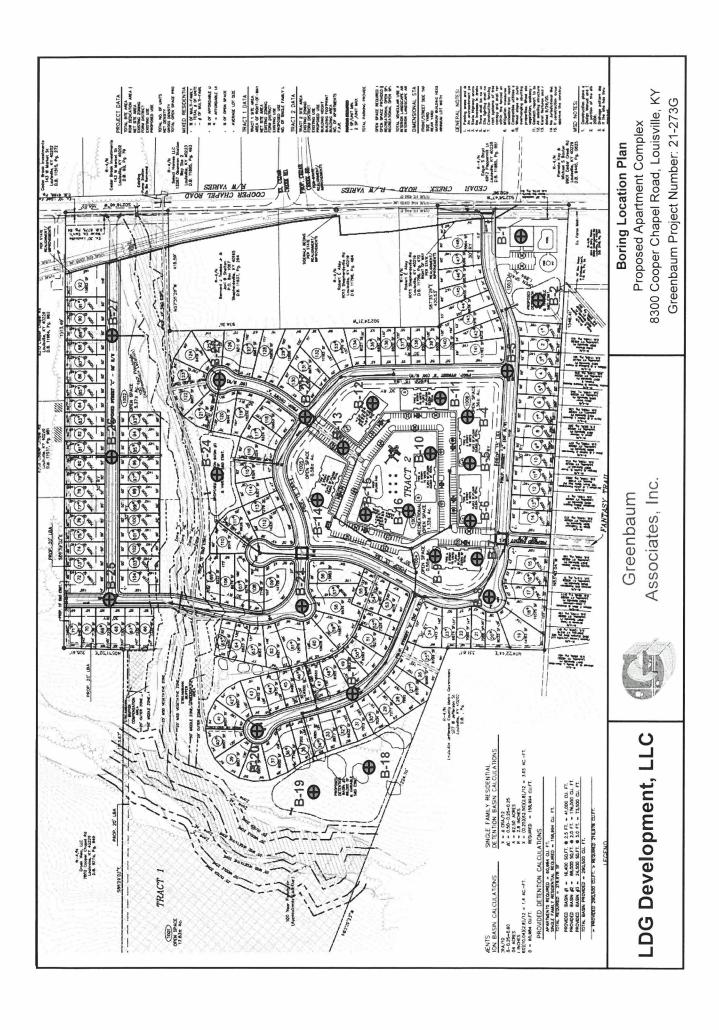
We strongly recommend that bearing surfaces and compaction be monitored by Greenbaum Associates, Inc. Our technicians will be available to further assist you in providing these and other normally specified quality control services. The report is preliminary until such time as these examinations are completed to confirm conditions consistent with those discovered in the investigation.

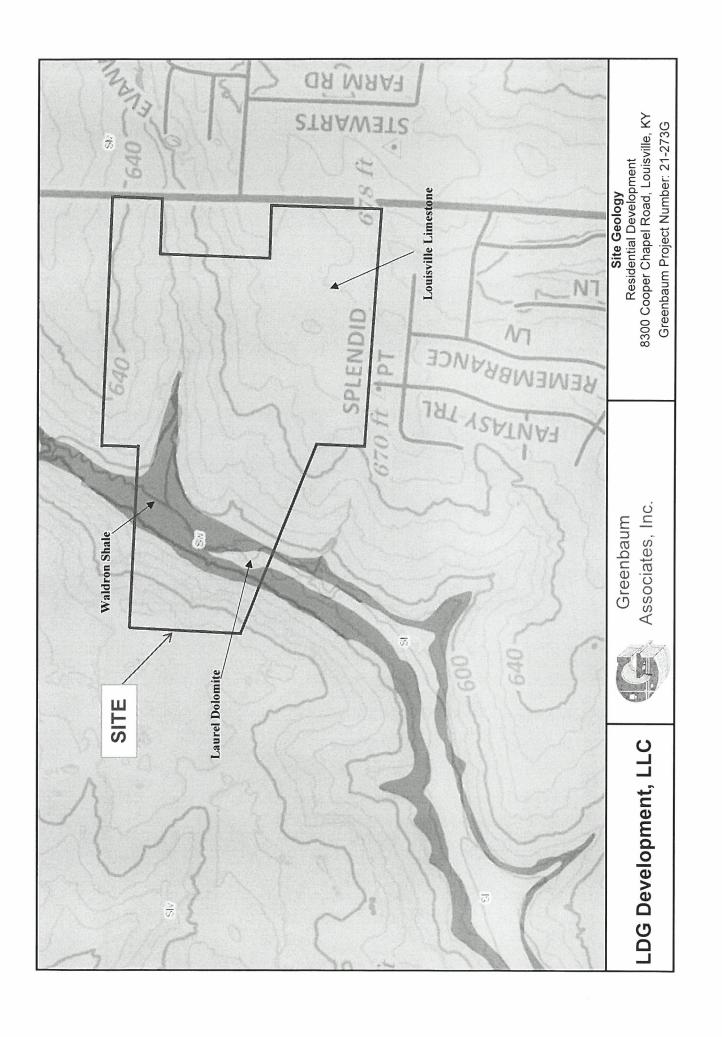
The conclusions and recommendations offered in this report are based on the subsurface conditions encountered in the borings. No warranties can be made regarding the continuity of conditions between or beyond borings. If, during construction, soil conditions are encountered that differ from those indicated in this report, a representative of Greenbaum Associates, Inc. should inspect the site to determining if design modification is required. In addition, only two borings were performed, this being a preliminary study. Additional borings and analysis will be required prior to final design and construction.

This study was directed at specific buildings and pavement at specific locations on this site to be constructed within a reasonably short period after this study. Use for any other location, structures or substantial changes in construction period may invalidate the recommendations. The geotechnical engineer should be consulted relative to any substantial change in these.

This study is directed at mechanical properties of the soils and includes no sampling, testing or evaluation for environmental considerations.







SOIL DESCRIPTION TERMINOLOGY

Soils are identified and classified in this report according the the Unified Classification System with the following modifiers:

RELATIVE DENSITY OF GRANULAR SOILS

CONSISTENCY OF COHESIVE SOILS

Description	Blows/Foot	Description	N-value	qu (tsf)
Very Loose	0 to 4	Very Soft	0 to 2	0 to 0.25
Loose	5 to 10	Soft	3 to 4	0.26 to 0.50
Medium Dense	11 to 30	Medium Stiff	5 to 8	0.51 to 1.0
Dense	31 to 50	Stiff	9 to 15	1.1 to 2.0
Very Dense	51 to 80	Very Stiff	16 to 30	2.1 to 4.0
Extremely Dense	81+	Hard	>30	4.1 to 8.0
		Very Hard		8.1+

PARTICAL SIZES

SOIL MOISTURE

Componen	<u>ts</u>	Size or Sieve No.		Descriptive Term
Boulders		over 12 inches	Dry	Dry of Standard Proctor Optimum
Cobbles		3 to 12 inches	Damp	Moist (sand only)
Gravel -	Coarse	3/4 to 3 inches	Moist	Near Standard Proctor Optimum
	Fine	No. 4 to ³ / ₄ inch	Wet	Wet of Standard Proctor Optimum
Sand -	Coarse	No. 10 to No. 4	Saturated	Free Water in Sample
	Medium	No. 40 to No. 10		
	Fine	No. 200 to No. 40		
Fines (silt a	ind clay)	Finer than No. 200		

ROCK DESCRIPTION TERMINOLOGY

The Rock Quality Determination (Deere et. Al., 1969) method of determining rock quality as reported here was obtained by summing up the total length of core recovered in each run, counting only those pieces of core which are four inches (10 cm.) in length or longer and which are hard and sound. The sum is then represented as a percentage over the length of the run. If the core is broken by handling or by the drilling process, the fresh broken pieces are fitted together and counted as one piece provided that they the requisite length of four inches (10 cm.). RQD is reported as a percentage.

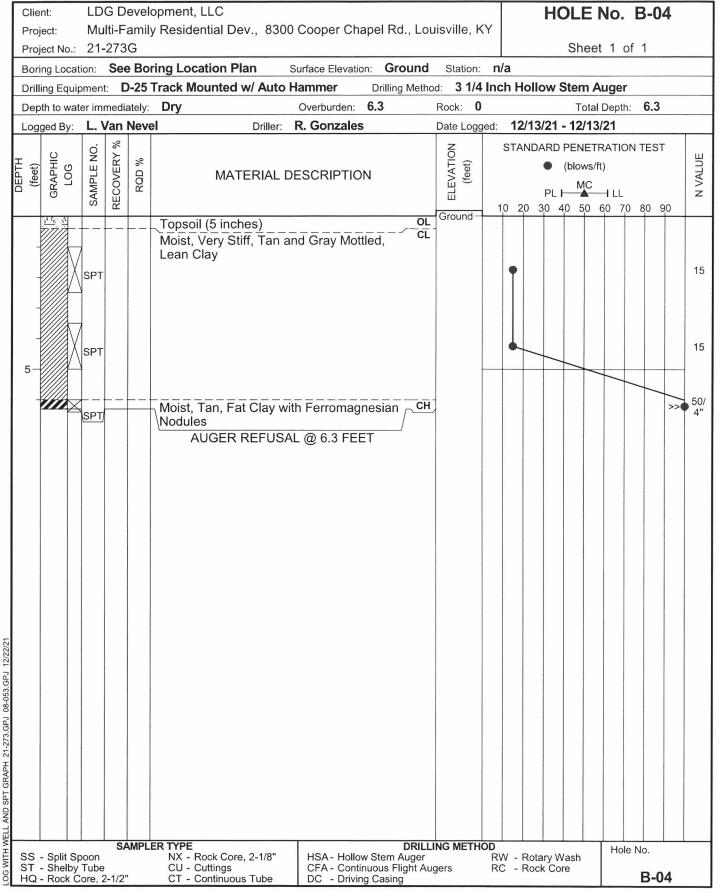
RELATIONSHIP BETWEEN RQD AND ROCK QUALITY

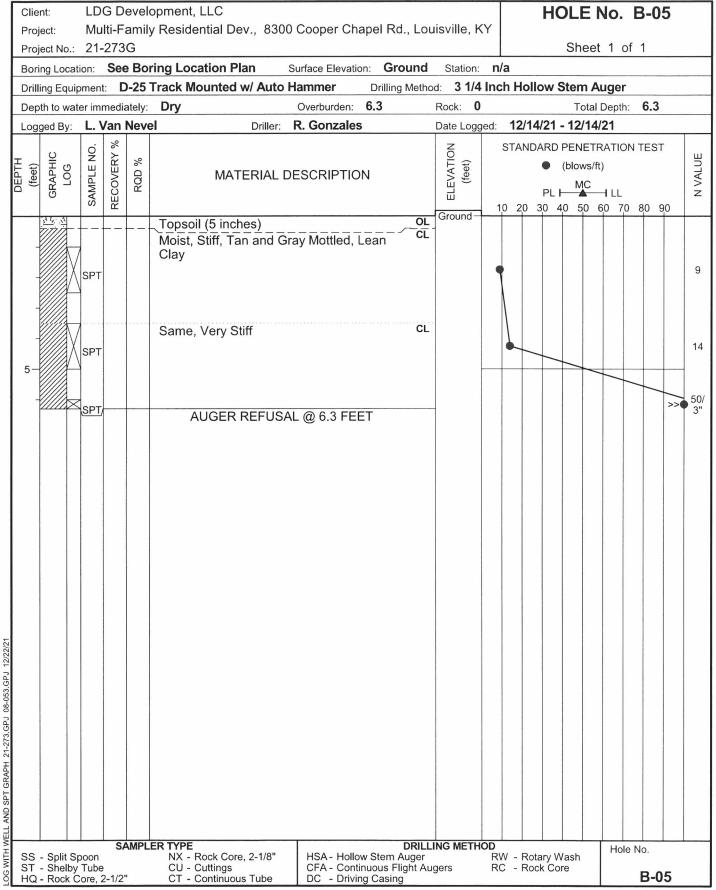
RQD (%)	Description of Rock Quality
0 to 25	Very Poor
26 to 50	Poor
51 to 75	Fair
76 to 90	Good
91 to 100	Excellent

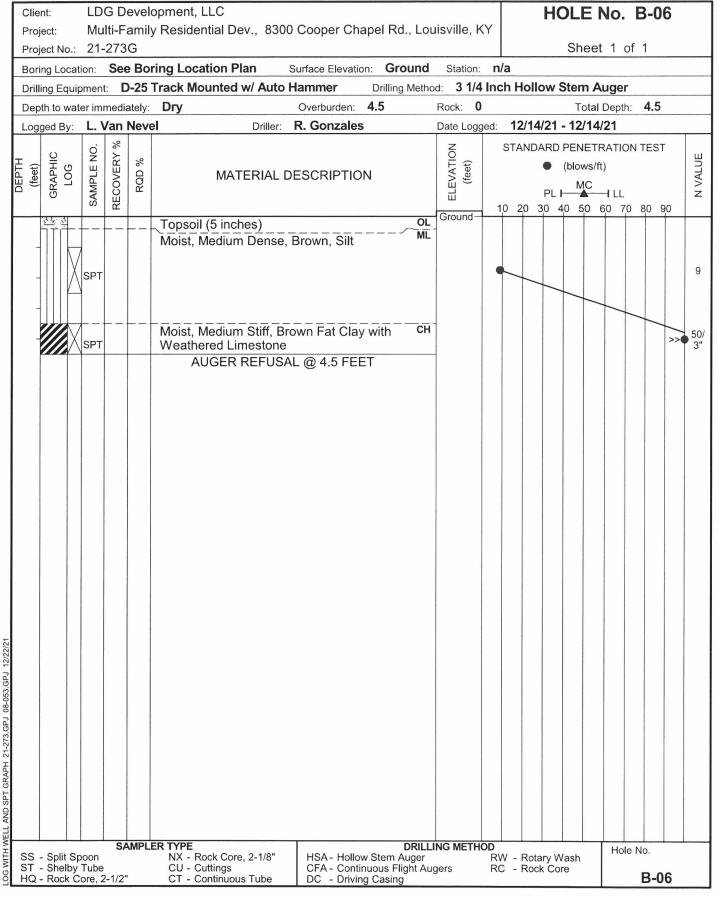
Clie					opment, LLC	Ohan	al Dal I av	ia illa IA	\prod	Н	DLE I	No. I	B-01	
Proj	ect: ect No.:				y Residential Dev., 8300 (Jooper Chape	ei Ra., Lou	iisviile, K			Sheet	1 of	1	
					ring Location Plan Su	rface Elevation:	Ground	Station:	n/a	·,		1 01		
					Track Mounted w/ Auto Ha		Drilling Metho			lollow	Stem A	uger		
	th to wat					Overburden: 7.	.7	Rock: 0			Total	Depth:	7.7	
Log	ged By:	L. \	/an	Neve	el Driller: R	. Gonzales		Date Logge	d: 12	2/13/21	- 12/13/	21		
DEPTH (feet)	GRAPHIC LOG	SAMPLE NO.	RECOVERY %	RQD %	MATERIAL DE	SCRIPTION		ELEVATION (feet)	STA	PL I	PENETF (blows/ft MC) - LL		
-		SPT			Topsoil (6 inches) Moist, Stiff, Tan, Fat Clay Ferromagnesian Nodules		OL CH	Ground						,
5-		SPT			Same, Very Stiff AUGER REFUSAL	@ 7.7 FEET	СН							
			97	MDI	ER TYPE		וומח	ING METHO	D					
	- Split Sp - Shelby			AVIF L	NX - Rock Core, 2-1/8" CU - Cuttings	HSA - Hollow S CFA - Continuo	item Auger		RW -	Rotary W Rock Co		Hole 1	VO.	
	- Rock C			•	CT - Continuous Tube	DC - Driving C	Casing	yerə	110 -	NOUR CO	16		B-01	

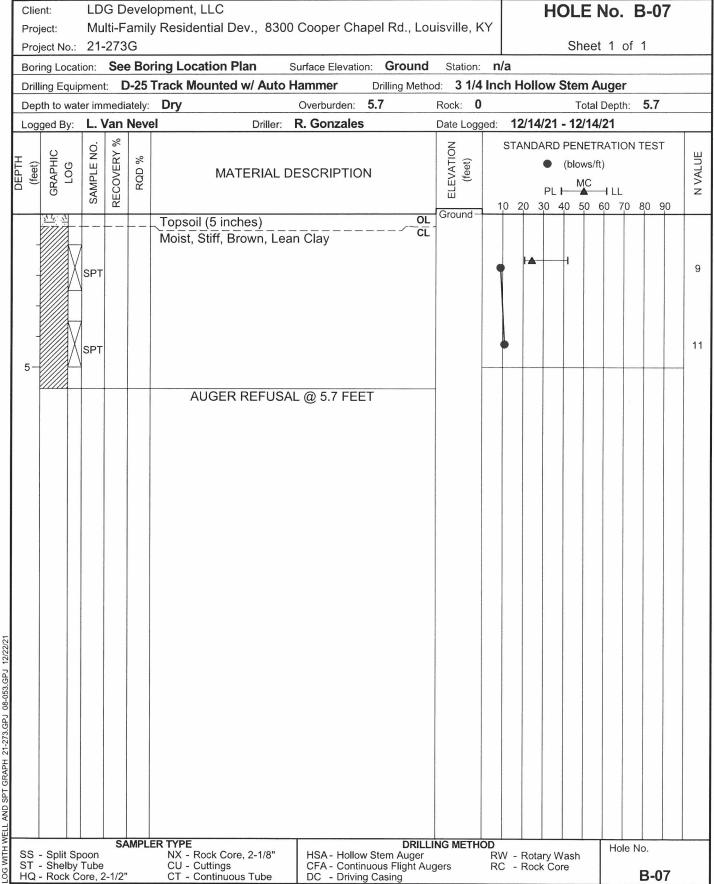
Clie Pro					opment, LLC y Residential Dev., 8300 Coo	ner Chanel Rd. Lou	ijsville K	_Y	Н	OLI	E No	. B-0)2	
	ect No.				y Nesidential Dev., 0000 000	per Onaper Na., Loc	iioviiio, iv			Sh	eet 1	of 1		
						e Elevation: Ground	Station:							
					Track Mounted w/ Auto Hamr			Inch H	Hollow				200	
	th to wa					burden: 1.6	Rock: 0				otal Dep	th: 1.6	<u> </u>	
Log	ged By:	<u>L.</u>		Neve	el Driller: R. G	onzales	Date Logge							_
_	ಲ	Š.	RECOVERY %	%			ELEVATION (feet)	STA	ANDAR			ON TES	T	Ļ
DEPTH (feet)	GRAPHIC	JE H	VEF	RQD %	MATERIAL DESC	RIPTION	EVATI (feet)		•		ws/ft)			
	GR.	SAMPLE NO.		R.					Pl	- I	IC I LI	_		:
	:47.· :1	S	<u> </u>			OL	Ground	10	20 30	40 5	0 60	70 80	90	_
	11.11.				Topsoil (5 inches)									
					Moist, Brown, Fat Clay with	Limestone CH								
-														
		1											>>	5
		SP				10555								
					AUGER REFUSAL @	1.6 FEET								
99	- Split 9	Snoor		AMPL	ER TYPE NX - Rock Core, 2-1/8" HS	DRILL SA - Hollow Stem Auger	ING METHO		Rotary	Wash	H	ole No.		_
ST	- Shelb	v Tub	е		CU - Cuttings CF	A - Continuous Flight Au	gers	RC -	Rock (Core		-	00	
HQ	- Rock	Core,	2-1/2	2"	CT - Continuous Tube DC	C - Driving Casing						B-	UZ	

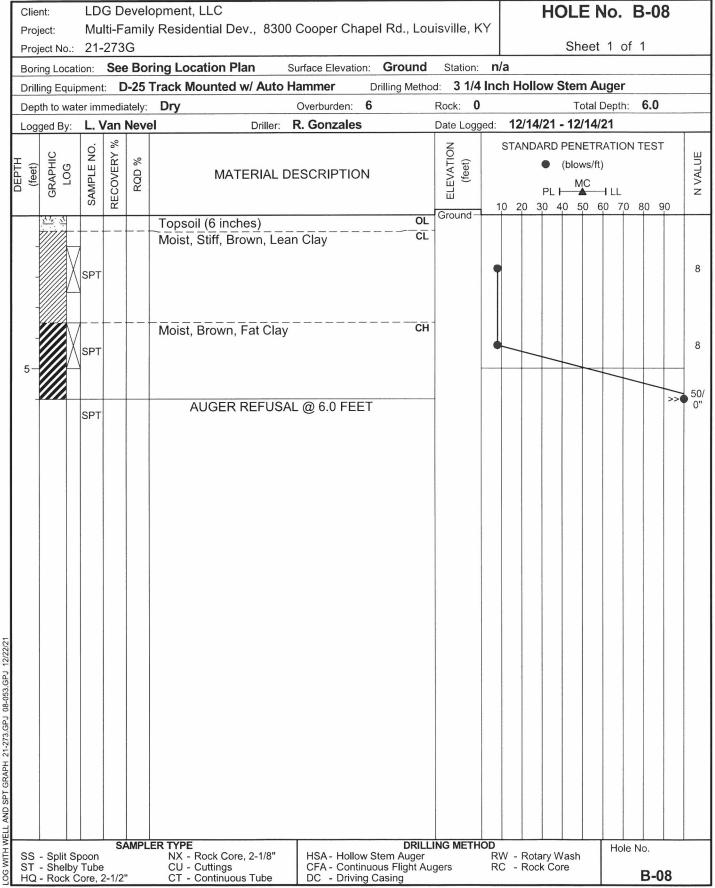
	Development, L	LC tial Dev., 8300 Cooper Chapel I	Rd., Louisville, K`		No. B-03	
Project No.: 21-2	73G			Shee	t 1 of 1	
	See Boring Loca					
				Inch Hollow Stem A		
Depth to water imm		Overburden: 5.5	Rock: 0		Depth: 5.5	
Logged By: L. Va		Driller: R. Gonzales		ed: 12/13/21 - 12/13		T
(feet) GRAPHIC LOG SAMPLE NO	RECOVERY %	MATERIAL DESCRIPTION	Punoron (feet)	STANDARD PENETI (blows/f PL MC 10 20 30 40 50	it) → LL	N VALUE
SPT		(5 inches) ledium Dense, Brown, Silt	OL Ground			18
SPT SPT	Moist, V	ery Stiff, Tan, Fat Clay	СН	•		19
SS - Split Spoon ST - Shelby Tube HQ - Rock Core. 2-						
SS - Split Spoon		ock Core, 2-1/8" HSA - Hollow Ster		RW - Rotary Wash	Hole No.	-
ST - Shelby Tube HQ - Rock Core, 2-	1/2" CT - Co	uttings CFA - Continuous ontinuous Tube DC - Driving Cas	Flight Augers ing	RC - Rock Core	B-03	





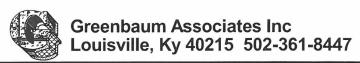




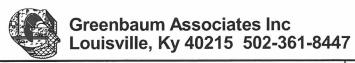


Project No.: 21-273G Sheet 1 of 1 Sheet 1 Sheet 1 of 1 Sheet 1 of 1 Sheet 1 of 1 Sheet 1 of 1 Sheet 1 Sheet 1 of 1 Sheet 1 of 1 Sheet 1 Sheet 1 of 1 Sheet 1 Sheet 1 of 1 Sheet
Drilling Equipment: D-25 Track Mounted w/ Auto Hammer Drilling Method: 3 1/4 Inch Hollow Stem Auger Depth to water immediately: Dry Overburden: 4.4 Rock: 0 Total Depth: 4.4 Logged By: L. Van Nevel Driller: R. Gonzales Date Logged: 12/14/21 - 12/14/21 MATERIAL DESCRIPTION MOIST, Stiff, Brown, Lean Clay Moist, Tan, Fat Clay with Ferromagnesian CH Nodules Dry Overburden: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 STANDARD PENETRATION TEST (blows/ft) PL MC (blows/ft) PL MC (blows/ft) Forumd Ground Moist, Stiff, Brown, Lean Clay SPT 12 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
Depth to water immediately: Dry Overburden: 4.4 Rock: 0 Total Depth: 4.4 Logged By: L. Van Nevel Driller: R. Gonzales Date Logged: 12/14/21 - 12/14/21 STANDARD PENETRATION TEST (blows/ft) MATERIAL DESCRIPTION MOIST, Stiff, Brown, Lean Clay SPT 6 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules Overburden: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 Rock: 0 Total Depth: 4.4 STANDARD PENETRATION TEST (blows/ft) PL MC LL 10 20 30 40 50 60 70 80 90 Ground Moist, Stiff, Brown, Lean Clay SPT 6 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
Date Logged: 12/14/21 - 12/14/21 STANDARD PENETRATION TEST (blows/ft) MATERIAL DESCRIPTION MOIST, Stiff, Brown, Lean Clay SPT 6 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules Date Logged: 12/14/21 - 12/14/21 STANDARD PENETRATION TEST (blows/ft) PL MC (blows/ft) Topsoil (6 inches) OL Moist, Stiff, Brown, Lean Clay CL Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
STANDARD PENETRATION TEST (blows/ft) MATERIAL DESCRIPTION Topsoil (6 inches) Moist, Stiff, Brown, Lean Clay Moist, Tan, Fat Clay with Ferromagnesian CH Nodules STANDARD PENETRATION TEST (blows/ft) PL MC 10 20 30 40 50 60 70 80 90 Ground SPT 12
Topsoil (6 inches) Moist, Stiff, Brown, Lean Clay SPT 12 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
Topsoil (6 inches) Moist, Stiff, Brown, Lean Clay SPT 12 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
Topsoil (6 inches) Moist, Stiff, Brown, Lean Clay SPT 12 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
Moist, Stiff, Brown, Lean Clay SPT 12 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
SPT 6 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
SPT 6 Moist, Tan, Fat Clay with Ferromagnesian CH Nodules
SPT 6 Nodules >>
AUGER REFUSAL @ 4.4 FEET
SAMPLER TYPE DRILLING METHOD Hole No.
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash
ST - Shelby Tube CU - Cuttings CFA - Continuous Flight Augers RC - Rock Core HQ - Rock Core, 2-1/2" CT - Continuous Tube DC - Driving Casing B-09

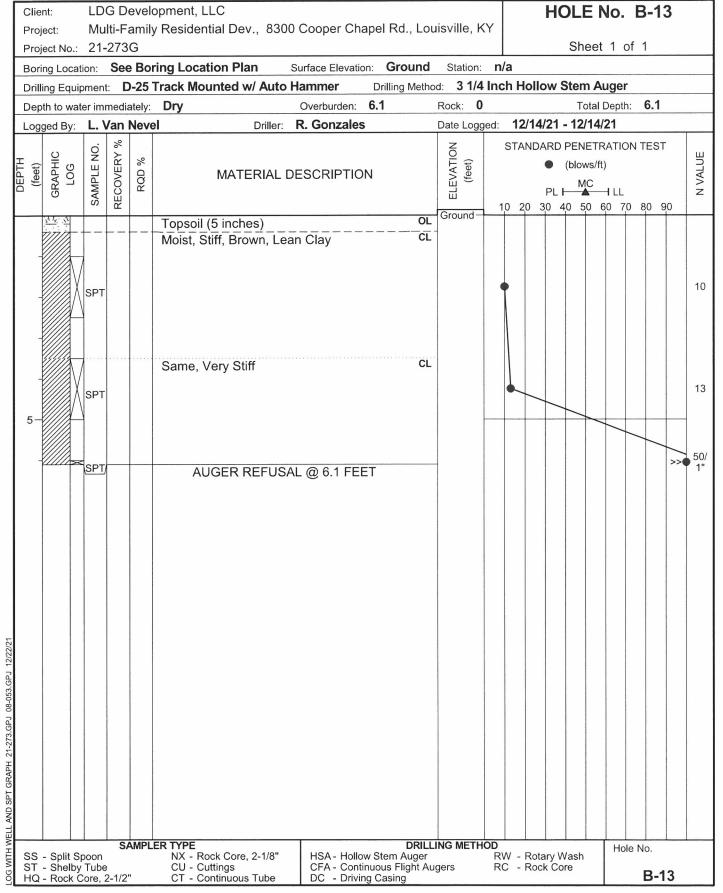
Clier	nt:	LD	G D	evelo	ppment, LLC					HOLE N	o. E	3-10	
Proje	ect:			•	Residential Dev., 8300	Cooper Chape	l Rd., Lou	iisville, KY	1				
Proje	ect No.:	21-	273							Sheet	1 of	1	
Bori	ng Locati	on:				urface Elevation:	Ground		n/a				
Drilli	ing Equip	ment	t: D	-25 7	rack Mounted w/ Auto H		rilling Metho		ch Hollo	w Stem Au			
	th to wate					Overburden: 6		Rock: 0		Total D		6.0	
Logg	ged By:	L. \	/an l	Neve	Driller: F	R. Gonzales		Date Logged	12/14/	21 - 12/14/2	!1		1
DEPTH (feet)	GRAPHIC LOG	SAMPLE NO.	RECOVERY %	RQD %	MATERIAL DE	ESCRIPTION		ELEVATION (feet)		RD PENETRA (blows/ft) MC PL MC 0 40 50 66	I LL		N VALUE
	17. 18 1 FZ				Topsoil (6 inches)		OL	Ground	10 20 0				
-		SPT			Moist, Medium Dense, T Mottled, Silt	an and Gray	ML						11
5-		SPT			Moist, Very Stiff, Tan, Fa Ferromagnesian Nodule		СН		•				12
SS - ST - HQ -					AUGER REFUSAL	. @ 6.0 FEET							
SS - ST -	- Split Sp	Tube	,		ER TYPE NX - Rock Core, 2-1/8" CU - Cuttings	HSA - Hollow S CFA - Continuo	tem Auger us Flight Au		RW - Rota		Hole N	o. B-10	
1100	- Rock C	J. C, 2	- 1/2		CT - Continuous Tube	DC - Driving C	Gonig						

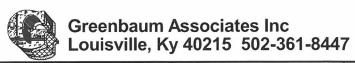


Client: Project:			opment, LLC y Residential Dev., 8300 Coo	ner Chanel Rd. Lou	ievilla KV	HOLE	No. B-11
-			y Residential Bev., 6000 000	oci onaperita., Loa	iioviiio, itti	Shee	et 1 of 1
Boring Location	on: Se	e Bo	ring Location Plan Surface	Elevation: Ground	Station: n	/a	
			Track Mounted w/ Auto Hamn			ch Hollow Stem	
Depth to water					Rock: 0		I Depth: 6.3
Logged By:		Neve	Driller: R. Go	onzales	Date Logged:	12/14/21 - 12/14	1/21
(feet) GRAPHIC LOG	SAMPLE NO. RECOVERY %	RQD %	MATERIAL DESCI	RIPTION	ELEVATION (feet)	STANDARD PENET (blows/ PL MC PL 20 30 40 50	ft)
-	SPT		Topsoil (5 inches) Moist, Medium Dense, Tan a Mottled, Silt	OL and Gray ML	Ground		
5-	SPT		Moist, Very Stiff, Dark Brown with Ferromagnesian Nodule				
	SPT/		Moist, Tan, Fat Clay	СН			>>•
			AUGER REFUSAL @ 6				
SS - Split Spo	oon	AMPLI	ER TYPE NX - Rock Core, 2-1/8" HS/	DRILLI A - Hollow Stem Auger	NG METHOD	W - Rotary Wash	Hole No.
ST - Shelby T HQ - Rock Co	Tube	! "	CU - Cuttings CF/	A - Continuous Flight Aug - Driving Casing	gers R0	C - Rock Core	B-11



	opment, LLC	uiovillo IVV	HOLE No. B-12	
Project: Multi-Family Project No.: 21-273G	/ Residential Dev., 8300 Cooper Chapel Rd., Lou	iisviiie, Ki	Sheet 1 of 1	
Boring Location: See Bor	ring Location Plan Surface Elevation: Ground	Station: n	/a	
Drilling Equipment: D-25	Track Mounted w/ Auto Hammer Drilling Metho		ch Hollow Stem Auger	
Depth to water immediately:		Rock: 0	Total Depth: 8.3	
Logged By: L. Van Neve	Priller: R. Gonzales	Date Logged:	12/14/21 - 12/14/21	
(feet) GRAPHIC LOG SAMPLE NO. RECOVERY % RQD %	MATERIAL DESCRIPTION	ELEVATIC (feet)	STANDARD PENETRATION TEST ● (blows/ft) PL MC	N VALUE
3/4:30	Topsoil (6 inches) OL	Ground		
SPT	Moist, Loose, Tan, Silt ML			8
5	Same, Medium Dense, Tan and Gray ML Mottled			13
SPT	AUGER REFUSAL @ 8.3 FEET			10
	ER TYPE DRILLI	NG METHOD	Hole No.	
SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2"	NX - Rock Core, 2-1/8" CU - Cuttings CT - Continuous Tube HSA - Hollow Stem Auger CFA - Continuous Flight Aug DC - Driving Casing	gers R(W - Rotary Wash C - Rock Core	in the second





Project Multi-Family Residential Dev., 8300 Cooper Chapel Rd., Louisville, KY Sheet 1 of 1	Clie					opment, LLC					H	HOL	ΕN	0.	B-1	4	
Boring Location: See Boring Location Plan Surface Elevation: Ground Station: n//a Drilling Equipment: D-25 Track Mounted w/ Auto Hammer Drilling Method: 3 1/4 Inch Hollow Stem Auger Total Depth: 8.3 Logged By: L. Van Nevel Driller: R. Gonzales Date Logged: 12/14/21 - 12/14/21 MATERIAL DESCRIPTION MATERIAL DESCRIPTION MOIST, Stiff, Brown, Lean Clay Moist, Stiff, Reddish Brown, Fat Clay AUGER REFUSAL @ 8.3 FEET Brownd AUGER REFUSAL @ 8.3 FEET		-			_	Residential Dev., 830	00 Cooper Chapel R	d., Loi	usville, K	Y		Sh	eet	1 of	1		
Depth to water immediately: Dry Overburden: 8.3 Rock: 0 Total Depth: 8.3						ring Location Plan	Surface Flevation: Gr	ound	Station:	n/a			CCI	1 01			
Logged By: L. Van Nevel Driller: R. Gonzales Date Logged: 12/14/21 - 12/14/21											Hollov	v Ster	n Au	ger			
SPT Moist, Stiff, Reddish Brown, Fat Clay SPT AUGER REFUSAL @ 8.3 FEET STANDARD PENETRATION TEST (blows/ft) Pt MC Pt MC Pt MC Topsoil (6 inches) Ground STANDARD PENETRATION TEST (blows/ft) Pt MC Topsoil (6 inches) Topsoil (6 inches) Ground Topsoil (6 inches) SPT SPT SPT Moist, Stiff, Reddish Brown, Fat Clay CH SPT SPT SPT SPT Moist, Stiff, Reddish Brown, Fat Clay CH SPT S	Dep	oth to wa	ter im	media	ately:	Dry	Overburden: 8.3		Rock: 0			Т	otal D	epth:	8.3		
Topsoil (6 inches) OL Ground SPT Moist, Stiff, Brown, Lean Clay Moist, Stiff, Reddish Brown, Fat Clay SPT AUGER REFUSAL @ 8.3 FEET	Log	ged By:	L. '	Van	Neve	Driller:	R. Gonzales		Date Logg	ed: 1	2/14/2	1 - 12	/14/2	1			
Topsoil (6 inches) OL Ground SPT Moist, Stiff, Brown, Lean Clay Moist, Stiff, Reddish Brown, Fat Clay SPT AUGER REFUSAL @ 8.3 FEET		0	o.	%					Z	ST	ANDAF	RD PEN	IETRA	TION	TES1		
Topsoil (6 inches) OL Ground SPT Moist, Stiff, Brown, Lean Clay Moist, Stiff, Reddish Brown, Fat Clay SPT AUGER REFUSAL @ 8.3 FEET	PTH et)	PHIC	LE	ÆR	% 0	ΜΔΤΕΡΙΔΙ	DESCRIPTION		/ATI(•	(blo	ws/ft)				YL UE
Topsoil (6 inches) OL Ground SPT Moist, Stiff, Brown, Lean Clay Moist, Stiff, Reddish Brown, Fat Clay SPT AUGER REFUSAL @ 8.3 FEET	DEI (fe	GRA	AMP	000	RQ	W TEN	DECORM FIGH		ELE)		Р	L	1C	LL			> Z
Moist, Stiff, Brown, Lean Clay SPT Moist, Stiff, Reddish Brown, Fat Clay CH SPT AUGER REFUSAL @ 8.3 FEET			S	8					-	10	20 30	40 5	0 60	70	80 9	90	
SPT Moist, Stiff, Reddish Brown, Fat Clay CH SPT AUGER REFUSAL @ 8.3 FEET		2/2	<u></u>														
Moist, Stiff, Reddish Brown, Fat Clay SPT SPT AUGER REFUSAL @ 8.3 FEET						Moist, Stiff, Brown, Le	ean Clay	CL									
Moist, Stiff, Reddish Brown, Fat Clay SPT SPT AUGER REFUSAL @ 8.3 FEET			Λ														
SPT SPT AUGER REFUSAL @ 8.3 FEET			SPT							•							8
SPT SPT AUGER REFUSAL @ 8.3 FEET			1														
SPT SPT AUGER REFUSAL @ 8.3 FEET																	
SPT SPT AUGER REFUSAL @ 8.3 FEET			 			Maint Office Dankink			-								
SPT SPT AUGER REFUSAL @ 8.3 FEET			/			Moist, Stiff, Readish E	Brown, Fat Clay	СП									
AUGER REFUSAL @ 8.3 FEET			SPT							1							9
AUGER REFUSAL @ 8.3 FEET	5-		1											_			
AUGER REFUSAL @ 8.3 FEET																	
AUGER REFUSAL @ 8.3 FEET																	
AUGER REFUSAL @ 8.3 FEET			/														
			SPT														10
			1														
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HSA - Hollow Stem Auger CU - Cuttings CT - Continuous Flight Augers CT - Continuous Flight Augers CT - Continuous Tube B-14 B-14						AUGER REFUS	AL @ 8.3 FEET										
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CU - Cuttings CT - Continuous Tube DRILLING METHOD HSA - Hollow Stem Auger CFA - Continuous Fight Augers RC - Rock Core DC - Driving Casing B-14																	
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SS - Split Spoon NX - Rock Core, 2-1/8" CFA - Continuous Flight Augers CFA - CONTINUOUS Flight																	
SAMPLER TYPE SS - Split Spoon NX - Rock Core, 2-1/8" ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube NA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - Continuous																	
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube NASA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - Rock Core DC - Driving Casing NASA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - Rock Core DC - Driving Casing NASA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - Rock Core DC - Driving Casing R-14	LZ/Z																
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SAMPLER TYPE HSA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - CONTINUOUS Flight	12/2																
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SAMPLER TYPE BRILLING METHOD HSA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - CO	3.GP,																
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SAMPLER TYPE HSA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - CONTINUOUS Flight	90-80																
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SAMPLER TYPE HSA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - CONTINUOUS Flight	S.GPJ																
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SAMPLER TYPE HSA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - CONTINUOUS Flight	21-27.																
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SAMPLER TYPE HSA - Hollow Stem Auger CFA - Continuous Flight Augers CFA - CONTINUOUS Flight A	APH																
SAMPLER TYPE SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2" CT - Continuous Tube SAMPLER TYPE HSA - Hollow Stem Auger CFA - Continuous Flight Augers DC - Driving Casing B-14 Hole No. B-14	E G																
SAMPLER TYPE SS - Split Spoon NX - Rock Core, 2-1/8" ST - Shelby Tube CU - Cuttings CFA - Continuous Flight Augers CFA - CON	ND SI																
SAMPLER TYPE SS - Split Spoon NX - Rock Core, 2-1/8" ST - Shelby Tube CU - Cuttings HQ - Rock Core, 2-1/2" CT - Continuous Tube DRILLING METHOD HSA - Hollow Stem Auger RW - Rotary Wash CFA - Continuous Flight Augers RC - Rock Core DC - Driving Casing Hole No. B-14	ELL A																
ST - Shelby Tube CU - Cuttings CFA - Continuous Flight Augers RC - Rock Core HQ - Rock Core, 2-1/2" CT - Continuous Tube DC - Driving Casing B-14	s S	- Split S	poon		AMPLI	NX - Rock Core, 2-1/8"	HSA - Hollow Stem	DRILL Auger	ING METH		- Rotary	/ Wash		Hole	No.		
	ST HQ	- Shelby	Tube	e 2-1/2'	,	CU - Cuttings	CFA - Continuous F	light Au	igers						B-1	4	

Client:					opment, LLC y Residential Dev., 8300	Cooper Chanc	al Dd. Lou	iieville K	<u></u>	HOLE	No. E	3-15	
Project Project					y Residential Dev., 6300	Cooper Chape	ei Ru., Lou	iisviiie, K		She	eet 1 of	1	
Boring	Locati	on:	Sec	Bo	ring Location Plan S	urface Elevation:	Ground	Station:	n/a				
					Track Mounted w/ Auto H				Inch H	ollow Stem			
						Overburden: 4.		Rock: 0			tal Depth:	4.5	
Logged	d By:	L. V		Neve	el Driller:	R. Gonzales		Date Logge	ed: 12 /	/14/21 - 12/	14/21		
(feet)	LOG	SAMPLE NO.	RECOVERY %	RQD %	MATERIAL DE	ESCRIPTION		ELEVATION (feet)	STA1	NDARD PENE (blow PL M PL 40 50	/s/ft)		N VALUE
317,	x .7				Topsoil (5 inches)		OL	Ground					
		SPT			Moist, Loose, Brown, Si	t	ML		•				6
		SPT			Moist, Medium Stiff, Bro	wn, Lean Clay	CL					>>•	50 0"
///					AUGER REFUSAL	@ 4.5 FEET							
SS - S ST - S			SA	MPL	ER TYPE NX - Rock Core, 2-1/8" CU - Cuttings	HSA - Hollow S CFA - Continuo	tem Auger	NG METHO	RW - F	Rotary Wash	Hole N		
HQ - R	Rock Co	ore, 2	-1/2"		CT - Continuous Tube	DC - Driving C						B-15	

	Development, LLC	eanar Chanal Dd. Law	iavilla IVV	HOLE	No. B-16
Project: Multi- Project No.: 21 - 27	Family Residential Dev., 8300 C	ooper Chapei Rd., Lou	isville, KY	Sheet	1 of 1
		face Elevation: Ground	Station: n/		
	D-25 Track Mounted w/ Auto Ha	mmer Drilling Metho	d: 3 1/4 Inc	h Hollow Stem A	uger
Depth to water imme	diately: Dry	verburden: 5.8	Rock: 0	Total	Depth: 5.8
Logged By: L. Va	- T T	Gonzales	Date Logged:	12/14/21 - 12/14	/21
(feet) (Reat) GRAPHIC LOG SAMPLE NO.	MATERIAL DES		ELEVATIC (feet)	STANDARD PENETF (blows/ft PL I Q 20 30 40 50 6	i)
- SPT	Topsoil (5 inches) Moist, Medium Dense, Br	OL own, Silt ML	Ground		1
5				.	1
SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1	SAMPLER TYPE NX - Rock Core, 2-1/8" CU - Cuttings /2" CT - Continuous Tube	DRILLI HSA - Hollow Stem Auger CFA - Continuous Flight Aug DC - Driving Casing	NG METHOD RV gers RC	V - Rotary Wash C - Rock Core	Hole No. B-16

	nt:				opment, LLC	01 1011	12		H	IOLE	No. E	3-17	
Pro	ject: ject No.:				/ Residential Dev., 8300 Coop	per Chapel Rd., Lo	buisville, K	Y		Shee	t 1 of	1	
					ring Location Plan Surface	e Elevation: Ground	Station:	n/a		01100		•	
					Track Mounted w/ Auto Hamm		nod: 3 1/4		Hollow	Stem A	uger		
Dep	th to wat	er imi	media	ately:	Dry Overb	burden: 3	Rock: 0			Total	Depth:	3.0	
Log	ged By:	L. \	/an	Neve	Driller: R. Go	onzales	Date Logge	ed: 1	12/15/2	1 - 12/15	/21		
DEPTH (feet)	GRAPHIC LOG	SAMPLE NO.	RECOVERY %	RQD %	MATERIAL DESCR	RIPTION	ELEVATION (feet)	SI	•	D PENETI (blows/f	t)	TEST	!
		S	꼾				Cround	10	20 30	40 50	60 70	80 90	_
-		SPT			Topsoil (5 inches) Moist, Medium Stiff, Brown, I		-	•					J
					AUGER REFUSAL @ 3								
99	- Split Sp	2002	SA	AMPL	ER TYPE NX - Rock Core, 2-1/8" HS.	DRIL A - Hollow Stem Auger	LING METHO	DD P\V	- Rotary	Mach	Hole N	No.	
ST	- Shelby - Rock C	Tube		,	CU - Cuttings CF	A - Continuous Flight A - Driving Casing	lugers	RC	- Rock (Core		B-17	

Client:				opment, LLC				HOLE	No. E	3-18	
Project:				Residential Dev., 8300 Cooper C	hapel Rd., Lοι	uisville, KY	´	01			
Project No				ing Location Dies	Cround	04-4:	7/2	Sne	et 1 of	1	
				ring Location Plan Surface Eleva Frack Mounted w/ Auto Hammer		Station:		ollow Stem	Augor		
Drilling Eq				***************************************		Rock: 0	nen n		al Depth:	3.5	
Logged By			Neve			Date Logge	d· 12	/15/21 - 12/1		0.0	
Logged D		8						NDARD PENE		TEST	
(feet) GRAPHIC	SAMPLE NO.	₽	%			ELEVATION (feet)	0171	(blows		LOT	픠
(feet)		RECOVERY	RQD %	MATERIAL DESCRIPTI	ON	EV/F		PL MC			N VALUE
_ 5	SAI	REC					10 2			30 90	2
1. N. 1.				Topsoil (5 inches)	OL	Ground					
				Moist, Stiff, Brown, Lean Clay	CL						
*////	\Box										
	 SPT						•				8
*////	/\ SFI										
*////											
/////				AUGER REFUSAL @ 3.5 FI	EET	1					
	*										
			AMPL	ER TYPE		ING METHO			Hole N	0.	
SS - Split ST - Shel	Spoon by Tub			NX - Rock Core, 2-1/8" HSA - Ho	llow Stem Auger ntinuous Flight Au		RW - I	Rotary Wash Rock Core			
HQ - Roc			"		ving Casing					B-18	

Client:		opment, LLC	Cooper Chanal Dd. Lo.	i a lilla IVV	HOLE	No. B-19	
Project: Project No.:		y Residential Dev., 8300	Cooper Chapel Rd., Lot	JISVIIIE, KY	Shee	t 1 of 1	
		ring Location Plan S	furface Elevation: Ground	Station: n		. 1 01 1	
		Track Mounted w/ Auto H			h Hollow Stem A	uger	
Depth to wat	er immediately:	Dry	Overburden: .7	Rock: 0	Total	Depth: 0.7	
Logged By:	L. Van Neve	Driller:	R. Gonzales	Date Logged:	12/15/21 - 12/15	/21	-
DEPTH (feet) GRAPHIC LOG	SAMPLE NO. RECOVERY % RQD %	MATERIAL DI		ELEVATIC (feet)	STANDARD PENET! (blows/fi PL MC PL 50 0 20 30 40 50	it) → LL	N VALUE
17 - 14 - 17		Topsoil (8 Inches)	OL	Ground			
12 · 22 · 15 ·		AUGER REFUSAI	L @ 0.7 FEET				
SS - Split Sp ST - Shelby HQ - Rock C	ooon Tube	ER TYPE NX - Rock Core, 2-1/8" CU - Cuttings CT - Continuous Tube	DRILL HSA - Hollow Stem Auger CFA - Continuous Flight Au DC - Driving Casing	ING METHOD R\ gers R(W - Rotary Wash C - Rock Core	Hole No. B-19	

LOG WITH WELL AND SPT GRAPH 21-273.GPJ 08-053.GPJ 12/22/21

Clie					opment, LLC	0 0 15		10		Н	OLE	No.	B-2	20	
Proj	ect: ect No.:		Iti-Fa 2730		Residential Dev., 8300	Cooper Chapel Ro	d., Lou	usville, K`	′		She	et 1	of 1		
_					ring Location Plan Su	urface Elevation: Gr	ound	Station:	n/a		0110	000	01 1		
					Track Mounted w/ Auto Ha	ammer Drilling	g Metho	od: 3 1/4	Inch H	ollow	Stem	Auge	r		
Dep	th to wat	er imi	media	ately:	Dry	Overburden: 3		Rock: 0			Tota	al Dept	h: 3.	0	
Log	ged By:	L. \	/an I	Neve	Driller: F	R. Gonzales		Date Logge	ed: 12	/15/21	- 12/1	5/21			T
DEPTH (feet)	<u></u> 5	SAMPLE NO.	RECOVERY %	RQD %	MATERIAL DE	SCRIPTION		Greet) (feet)		• PL	(blows MC 40 50	/ft) LL			N VALUE
_		SPT			Topsoil (4 inches) Moist, Hard, Brown, Lea and Limestone	n Clay with Sand	OL CL	Ground		•					24
COS WITH WELL AND SPT GRAPH 21-273.5P7 08-053.9P7 12/22/21 D S S D S S S S S S S S S S S S S S S			SA	Wbi	AUGER REFUSAL	@ 3.0 FEET	DRILL	ING METHO							
SS ·	- Split Sp - Shelby	Tube			ER TYPE NX - Rock Core, 2-1/8" CU - Cuttings	HSA - Hollow Stem A	Auger light Au	ING METHO gers	D RW - I RC - I	Rotary \	Vash ore	Но	le No.	00	
HQ.	Rock C	ore, 2	2-1/2"		CT - Continuous Tube	DC - Driving Casin	g					\bot	R-	20	

	lient: roject:					opment, LLC y Residential Dev., 8300	Cooper Chape	el Rd., Lou	ıisville, K	/	Н	OLE	No.	B-:	21	
Pr	roject No											Shee	et 1 d	of 1		
							ırface Elevation:		Station:		la II acce	04	•			
						Track Mounted w/ Auto H	Overburden: 6	Orilling Metho	Rock: 0	ncn F	10IIOW		Auger I Depth		n	
	epth to w						R. Gonzales		Date Logge	d: 11	2/14/21			1. 0.	<u> </u>	-
LC	Jgged by	$\neg \top$		%	100	Dillier.	. Oonzaics				ANDARD			NI TE		Τ
DEPTH	(feet) GRAPHIC	3	SAMPLE NO.	RECOVERY 6	RQD %	MATERIAL DE	SCRIPTION		ELEVATION (feet)	317	•	(blows	ft)		51	N VALUE
	l <u>p</u>		SAN	REC	L.					10 3	PL 20 30				90	Z
	11/2 1/1	\top				Topsoil (5 inches)		OL	Ground	<u> </u>					1	
		T				Moist, Stiff, Brown, Lean	Clay	CL	1							
			РТ							•						11
		$/ \parallel^{3}$	FI													
										-						
		1				Same, with Weathered I	imestone	CL								
			РТ													13
		//	FI													
5												$\dagger \dagger$			1	1
	<i>Y/////</i>	T				AUGER REFUSAL	@ 6.0 FEET		1							
SS	S - Split	Spo	on	SA	MPL	ER TYPE NX - Rock Core, 2-1/8"	HSA - Hollow S	Stem Auger	ING METHO		Rotary V	Vash	Hol	e No.	•	
ST	T - Shell Q - Rock	by Ti	ube	-1/2"		CU - Cuttings CT - Continuous Tube	CFA - Continuo DC - Driving C	ous Flight Au	gers	RC -	Rock Co	ore		В	21	

Sheet 1 of 1 Shee	Client:				ppment, LLC		HOLE No. B-2	22
Borring Location: See Boring Location Plan Surface Elevation: Ground Station: n/a	Project:				Residential Dev., 8300 Cooper Chapel Rd	I., Louisville, K		
Depth to water immediately Dry								
Depth to water immediately: Dry			_					
Logend By: L. Van Nevel Driller: R. Gonzales Date Loggod: 12/15/21 - 12/15/21								•
MATERIAL DESCRIPTION MATERIAL DESCRIPTION MATERIAL DESCRIPTION MATERIAL DESCRIPTION MATERIAL DESCRIPTION Topsoil (5 inches) Moist, Stiff, Reddish Brown, Lean Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules AUGER REFUSAL @ 7.6 FEET SAMPLER TYPE NX. Rock Core, 2-1/8* HSA- Hollow Stem Auger RW Rotary Wash Hollo No.		***************************************)
MATERIAL DESCRIPTION MATERIAL DESCRIPTION Moist, Very Stiff, Reddish Brown, Lean Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET Moist, Very Stiff, Reddish Brown, Fat Clay Moist, Very St	Logged By:			Neve	Driller: R. Gonzales			_
Topsoil (6 inches) Moist, Siff, Reddish Brown, Fat Clay Moist, Very Stiff, Reddish Brown, Fat Clay CH With Ferromagnesian Nodules AUGER REFUSAL @ 7.6 FEET Same, with Weathered Limestone CH AUGER REFUSAL @ 7.6 FEET DRILLING METHOD NX - Rock Core, 2-1/8* HSA- Hollow Stem Auger HOLE NO.	∓ () ∃	N O		%		NOIT (2)		1 4
Topsoil (6 inches) Moist, Siff, Reddish Brown, Fat Clay Moist, Very Stiff, Reddish Brown, Fat Clay CH With Ferromagnesian Nodules AUGER REFUSAL @ 7.6 FEET Same, with Weathered Limestone CH AUGER REFUSAL @ 7.6 FEET DRILLING METHOD NX - Rock Core, 2-1/8* HSA- Hollow Stem Auger HOLE NO.	(feet) SRAPHI	IPLE	OVE	Q	MATERIAL DESCRIPTION	EVA.		VAL
Topsoil (5 inches) Moist, Stiff, Reddish Brown, Lean Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules Same, with Weathered Limestone CH AUGER REFUSAL @ 7.6 FEET PRILLING METHOD NX - Rock Core, 2-1/8* HSA- Hollow Stem Auger HOLL NO METHOD RW - Rotary Wash Holle No.	9	SAN	ZEC.	LE		日		
Moist, Stiff, Reddish Brown, Lean Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules Moist, Very Stiff, Reddish Brown, Fat Clay With Ferromagnesian Nodules Same, with Weathered Limestone CH AUGER REFUSAL @ 7.6 FEET DRILLING METHOD NX - Rock Core, 2-1/8* HSA- Hollow Stem Auger HOLE NO.	17. X1 12.				Topsoil (5 inches)	OL Ground	10 20 30 40 30 60 70 80	90
Moist, Very Stiff, Reddish Brown, Fat Clay CH with Ferromagnesian Nodules Same, with Weathered Limestone CH SPT AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET BAMPLER TYPE NX - Rock Core, 2-1/8" HSA- Hollow Stem Auger RW - Rotary Wash Hole No.		_			Moist, Stiff, Reddish Brown, Lean Clay	CL		
Moist, Very Stiff, Reddish Brown, Fat Clay CH with Ferromagnesian Nodules SPT Same, with Weathered Limestone CH SPT AUGER REFUSAL @ 7.6 FEET SAMPLER TYPE NX - Rock Core, 2-1/8" HSA- Hollow Sitem Auger RW - Rotary Wash Hole No.		1			with Ferromagnesian Nodules			
Moist, Very Stiff, Reddish Brown, Fat Clay CH with Ferromagnesian Nodules SPT Same, with Weathered Limestone CH SPT AUGER REFUSAL @ 7.6 FEET SAMPLER TYPE NX - Rock Core, 2-1/8" HSA- Hollow Sitem Auger RW - Rotary Wash Hole No.								1 1
SAMPLER TYPE SAMPLER TYPE NX - Rock Core, 2-1/8*		SPT						
SAMPLER TYPE SAMPLER TYPE NX - Rock Core, 2-1/8*								
SAMPLER TYPE SAMPLER TYPE NX - Rock Core, 2-1/8*								
SAMPLER TYPE SS - Split Spoon SAMPLER TYPE NX - Rock Core, 2-1/8" NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash Hole No.		 			Moist, Very Stiff, Reddish Brown, Fat Clay	CH		
Same, with Weathered Limestone CH AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET DRILLING METHOD NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash Hole No.		CDT						16
AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET BRILLING METHOD NX - Rock Core, 2-1/8" HSA- Hollow Stem Auger RW - Rotary Wash Hole No.		SPI						
AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET BRILLING METHOD NX - Rock Core, 2-1/8" HSA- Hollow Stem Auger RW - Rotary Wash Hole No.	5-							
AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET BRILLING METHOD NX - Rock Core, 2-1/8" HSA- Hollow Stem Auger RW - Rotary Wash Hole No.								
AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET BRILLING METHOD NX - Rotary Wash NX - Rotary Wash Hole No.		1			Same, with Weathered Limestone	СН		
AUGER REFUSAL @ 7.6 FEET AUGER REFUSAL @ 7.6 FEET BRILLING METHOD NX - Rotary Wash NX - Rotary Wash Hole No.		SDT						20
SAMPLER TYPE SS - Split Spoon SAMPLER TYPE NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash Hole No.	- //// /\							
SAMPLER TYPE SS - Split Spoon SAMPLER TYPE NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash Hole No.					AUGER REFUSAL @ 7.6 FEET			
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash					_			
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash								
SS - Split Spoon NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger RW - Rotary Wash				A.F.	TO TUDE	DDII I I I I I I I I I I I I I I I I I		
				AMPLE	NX - Rock Core, 2-1/8" HSA - Hollow Stem A	luger	RW - Rotary Wash	
ST - Shelby Tube CU - Cuttings CFA - Continuous Flight Augers RC - Rock Core DC - Driving Casing B-22	ST - Shelby HQ - Rock C	Tube ore, 2	!-1/2"				RC - Rock Core	22

			opment, LLC / Residential Dev., 8300 Cooper Chapel Rd., Lo	uiovillo KV	HOLE	No. B-23	
	1-273		Residential Dev., 6300 Cooper Chaper Nd., Lo	uisville, KT	Sheet	1 of 1	
Boring Location	: See	Во	ring Location Plan Surface Elevation: Ground	Station: r	ı/a		
Drilling Equipme	ent: D	-25			ch Hollow Stem A		
Depth to water i				Rock: 0		Depth: 1.5	
Logged By: L		Neve	Driller: R. Gonzales		12/15/21 - 12/15/		
(feet) (ReapHIC LOG	SAMIPLE NO. RECOVERY %	RQD %	MATERIAL DESCRIPTION		STANDARD PENETF (blows/ft PL MC PL A) -1 LL	N VALUE
SE SE			Topsoil (5 inches) Moist, Brown, Lean Clay with Weathered Limestone AUGER REFUSAL @ 1.5 FEET	Ground		>>•	50/0"
		MPL		ING METHOD		Hole No.	
SS - Split Spoo ST - Shelby Tu HQ - Rock Core	ıbe		NX - Rock Core, 2-1/8" HSA - Hollow Stem Auger CU - Cuttings CFA - Continuous Flight At CT - Continuous Tube DC - Driving Casing		RW - Rotary Wash RC - Rock Core	B-23	

	Development, LLC Family Residential Dev., 8300 0	Cooper Chanal Pd. Lou	ijevillo KV	HOLE N	lo. B-24	
Project No.: 21-273		Dooper Chaper No., Loc	iisviiie, itti	Sheet	1 of 1	
	ee Boring Location Plan Su	rface Elevation: Ground	Station: n /	'a		
	D-25 Track Mounted w/ Auto Ha	ammer Drilling Metho	d: 3 1/4 Inc	h Hollow Stem Au	ıger	
Depth to water immed	diately: Dry	Overburden: 3.9	Rock: 0	Total D	Depth: 3.9	
Logged By: L. Van	Nevel Driller: F	R. Gonzales	Date Logged:	12/15/21 - 12/15/2	21	_
(feet) GRAPHIC LOG SAMPLE NO. RECOVERY %	% MATERIAL DE		ELEVATIC (feet)	STANDARD PENETR/ (blows/ft) PL MC PL 0 20 30 40 50 66	I LL	AL IAV N
SPT	Moist, Medium Stiff, Brov		Ground		>>•	50
SS - Split Spoon ST - Shelby Tube HQ - Rock Core. 2-1/2						
SS - Split Spoon ST - Shelby Tube HQ - Rock Core, 2-1/2	AMPLER TYPE NX - Rock Core, 2-1/8" CU - Cuttings CT - Continuous Tube	DRILLI HSA - Hollow Stem Auger CFA - Continuous Flight Αυφ DC - Driving Casing		V - Rotary Wash	Hole No. B-24	

Clie	ent:				opment, LLC				H	OLE N	lo. B-	-25	
	ject:				y Residential Dev., 8300	Cooper Chape	I Rd., Loι	iisville, KY		Shoot	1 of 1		
	ject No.:				ring Location Plan S	Surface Elevation:	Ground	Station: r	 n/a	Sileet	1 01 1		\dashv
					Track Mounted w/ Auto H			d: 3 1/4 In		/ Stem A	uger		
	oth to wate			-		Overburden: 3.2		Rock: 0				.2	
	ged By:					R. Gonzales		Date Logged:	12/15/2	1 - 12/15/	21		
DEPTH (feet)	GRAPHIC LOG	SAMPLE NO.	RECOVERY %	RQD %	MATERIAL DI	ESCRIPTION		ELEVATION (feet)	•	D PENETF (blows/ft MC 40 50 6) LL		N VALUE
	71 N 1/1				Topsoil (5 inches)		OL	Ground					
		SPT			Moist, Reddish Brown, I Weathered Limestone	Lean Clay with	CL					>>(50/ 5"
					AUGER REFUSAI	L @ 3.2 FEET							
SS	- Split Sp	oon		MPL	ER TYPE NX - Rock Core, 2-1/8"	HSA - Hollow St	em Auger	ING METHOD	RW - Rotary		Hole No.		
ST HQ	ShelbyRock C	Tube ore, 2	: 2-1/2"		CU - Cuttings CT - Continuous Tube	CFA - Continuo DC - Driving C	us Flight Au asing	gers F	RC - Rock (Core	В	3-25	

LOG WITH WELL AND SPT GRAPH 21-273.GPJ 08-053.GPJ 12/22/21

Client:			opment, LLC	_				HOLE	No. E	3-26	
Project: Project No.:			y Residential Dev., 8300	Cooper Chape	I Rd., Lou	iisville, KY		Shor	et 1 of	1	
			ring Location Plan S	urface Elevation:	Ground	Station: r	⊓/a	31166		1	-
			Track Mounted w/ Auto H			d: 3 1/4 In		w Stem	Auger		
Depth to wat				Overburden: 1		Rock: 0				1.0	
Logged By:				R. Gonzales		Date Logged:	12/15/	21 - 12/1	5/21		
(feet) GRAPHIC LOG	SAMPLE NO. RECOVERY %	RQD %	MATERIAL DE	ESCRIPTION		ELEVATION (feet)		(blows			N VALUE
1, 1, 1, 1			Topsoil (6 inches)	State of the state	OL	Ground	10 20 3	0 40 30	1 1	1 1	
			Moist, Brown, Lean Clay		CL	1					
			AUGER REFUSAL								
		ΔΜΡΙ	FR TYPF		DRILL	ING METHOD					
SS - Split S	ooon	AMPL	ER TYPE NX - Rock Core, 2-1/8"	HSA - Hollow St	em Auger	ING METHOD	RW - Rota	ry Wash	Hole N	0.	
ST - Shelby HQ - Rock C	Tube		CU - Cuttings CT - Continuous Tube	CFA - Continuou DC - Driving C	us Flight Au asing	gers F	RC - Rock	Core		B-26	

LOG WITH WELL AND SPT GRAPH 21-273.GPJ 08-053.GPJ 12/22/21

Client:				opment, LLC	0 01	IDI I		,	HC)LE i	No.	B-27	7
Project: Project No.:				y Residential Dev., 8300	Cooper Chape	ei Ka., Lot	iisviiie, K t			Sheet	1 of	1	
				ring Location Plan S	urface Elevation:	Ground	Station:	n/a					
Drilling Equip	pment	: D	-25	Track Mounted w/ Auto H	lammer D	rilling Metho	d: 3 1/4 I	nch H	ollow S	Stem A	uger		
Depth to wat					Overburden: 3.	3	Rock: 0				Depth:	3.3	
Logged By:	L. V		Neve	Driller:	R. Gonzales		Date Logge	d: 12 /	15/21 -	12/15	21		
(feet) GRAPHIC LOG	SAMPLE NO.	RECOVERY %	RQD %	MATERIAL DI	ESCRIPTION		ELEVATION (feet)	STA1	• PL F	PENETF (blows/ft MC 0 50 6	:) - LL		0
1/2 1/2				Topsoil (6 inches)		OL	Ground						
	SPT			Moist, Brown, Lean Clay	y	CL							>>•
				AUGER REFUSAL	_ (W 3.3 FEE								
SS - Split S	noon	SA	MPLI	ER TYPE NX - Rock Core, 2-1/8"	HSA - Hallow S		NG METHO		Potor: \^	ach	Hole I	No.	
SS - Split Sp ST - Shelby HQ - Rock C	Tube	!-1/2"		CU - Cuttings CT - Continuous Tube	HSA - Hollow S CFA - Continuo DC - Driving C	us Flight Aug	gers		Rotary W Rock Cor			B-27	7

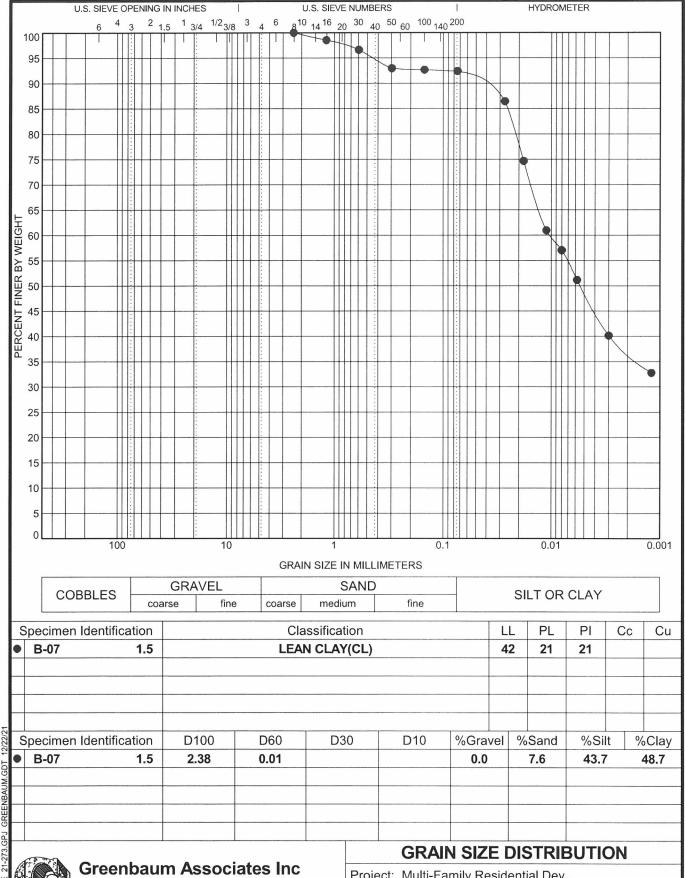
CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES ASTM D2487 and D2488 Group **Laboratory Classification Criteria Major Divisions Typical Names Symbols Gravels** (More than half of coarse fraction Determine percentages of sand and gravel from grain-size curve. Depending Clean Gravels (Little or $C_u = D_{60}/D_{10}$ greater than 4 Well-graded gravels, gravel-sand Coarse-grained soils (More than half of material is larger than No symbols GW $C_{11} = (D_{30})^{2}/(D_{10} \times D_{60})$ between 1 and 3 mixtures, little or no fines on percentage of fines (fraction smaller that No. 200 sieve size), coarselarger than No. 4 sieve) Not meeting all gradation requirements for Poorly graded gravels, gravel-sand dual **GP** mixtures, little or no fines requireing Appreciable amount d Atterberg limits below **Gravels with fines GM**^a Silty gravels, gravel-sand-silt mixtures "A" line with P. I. less Above "A" line with P. of fines) than 4 I. between 4 and 7 are Borderline cases GP, SW, SP GM, GC, SM, SC borderline cases Atterberg limits below Clayey gravels, gravel-sand-clay 200 sieve size) GC requireing us of dual "A" line with P. I. mixtures greater than 7 symbols Sands (More than half of coarse fraction is Clean Sands (Little or GW, $C_u = D_{60}/D_{10}$ greater than 6 Well-graded sands, gravelly sands, grained soils are classified as follows: SW little or no fines $C_u = (D_{30})^2 / (D_{10} \times D_{60})$ between 1 and 3 no fines) smaller than No. 4 sieve size) Poorly graded sands, gravelly sands, Not meeting all gradation requirements for SP little or no fines SW More than 12 percent Less than 5 percent Appreciable amount d Limits plotting in hatched with fines percent SMa Silty sands, sand-silt mixtures Atterberg limits above zone with P.I. between 4 of fines) "A" line or P.I. < 4 and 7 are borderline cases 5 to 12 Atterberg limits above requireing use of dual SC Clayey sands, sand-clay mixtures "A" lime with P.I. > 7 symbols Inorganic silts and very fine sands, Fine-grained soils (More than half meterial is smaller than (Liquid limit less than 50) ML silty or clayey fine sands, or clayey silts with slight plasticity Silts and clays Inorganic clays of low to medium CL plasticity, gravelly clays, sandy clays, silty clays, lean clays Organic silts and organic siltyclays of (%) OL low plasticity Plasticity Index No. 200 sieve) Inorganic silts, micaceous or (Liquid limit less that 50) MH diatomaceous fine sand or silty soils, elastic silts Silts and clays 20 Inorganic slays of high plasticity, fat CH MH 10 clays ML -CL-M ML Organic clays of medium to high OH 20 10 100 plasticity, organic silts Liquid Limit (%) organic Plasticity Chart Highly

Peat and other highly organic soils

Pt

^a Division of GM and SM groups into subdivisions of d and u are for roads and airfields only. Subdivision is based on Atterberg limits :suffix d used when L. L. is 28 or less and the P. I. is 6 or les; the suffix u used when L. L. is greater than 28.

^b Borderline classifications, used for soils possessing characeristics of two groups, are designated by combinations of group symbols. For exampls: GW-GC, well-graded gravel-sand misture with clay binder.

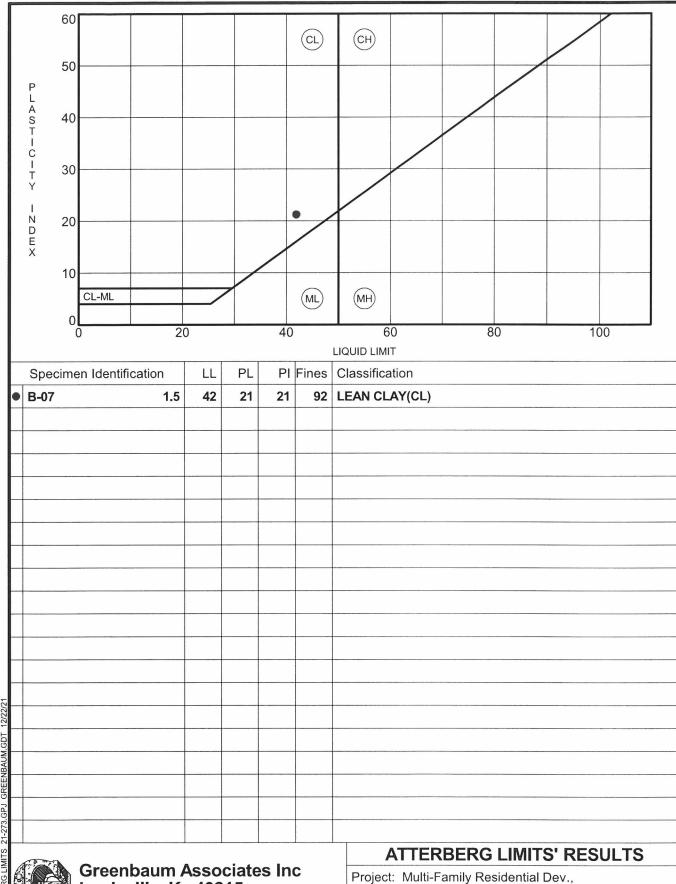


Louisville, Ky 40215 502-361-8447

Project: Multi-Family Residential Dev.,

Location: 8300 Cooper Chapel Rd., Louisville, KY

Number: 21-273G



L 5

Greenbaum Associates Inc Louisville, Ky 40215 502-361-8447

Location: 8300 Cooper Chapel Rd., Louisville, KY

Number: 21-273G