

ECS Southeast, LLP

Geotechnical Engineering Report

Tucker Station Road Property

Tucker Station Road Louisville, Jefferson County, Kentucky 40299

ECS Project Number 61:2606

December 22, 2021



"Setting the Standard for Service"



Geotechnical • Construction Materials • Environmental • Facilities

December 22, 2021

Xebec Realty 2100 Ross Avenue, Suite 895 Dallas, Texas 75201

Attention: Mr. Jake Spring, Vice President of Acquisitions

ECS Project No. 61:2606

Reference: **Geotechnical Engineering Report Tucker Station Road Property Tucker Station Road** Louisville, Jefferson County, Kentucky 40299

Dear Mr. Spring:

ECS Southeast, LLP (ECS) has completed the subsurface exploration and geotechnical engineering analyses for the above-referenced project. Our services were performed in general accordance with ECS Proposal No. 61:P2474, dated September 22, 2021.

This report presents our understanding of the geotechnical aspects of the project along with the results of the field exploration, laboratory testing conducted, and our geotechnical related design and construction recommendations.

It has been our pleasure to be of service to Xebec Realty during the design phase of this project. We would appreciate the opportunity to remain involved during the continuation of the design phase and would like to provide our services during construction operations as well to confirm the interpreted subsurface conditions utilized in this report. Should you have any questions concerning the information contained in this report, or if we can be of further assistance to you, please contact the writers.

Respectfully submitted,

ECS Southeast, LLP

B. Hasanguchelf

Bashir Hasanzadeh, Ph.D. Project Engineer Bhasanzadeh@ecslimited.com



John D. Godfrey Jr., P.E. **Principal Engineer**

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EXECUTIVE SUMMARY

This Executive Summary presents as a very brief overview of the geotechnical conditions at this site that are expected to affect design and construction. The following conditions were characteristic of the encountered site and subsurface conditions:

- The site is an approximately 108 acres of land on Tucker Station Road in Louisville, Kentucky and consists of wooded areas, agricultural fields, several buildings (residential houses) and outbuildings, access roads and driveways, a creek/swale, an existing stockpile of construction debris (mainly crushed asphalt), and an existing pond. The site is undulating but generally sloped downward to the south of the site with a maximum elevation difference of approximately 20 to 30 feet within the proposed building footprints.
- Surface materials generally consisted of approximately 1 to 21 inches of topsoil. The thicker areas of topsoil were located within the agriculturally disturbed areas. In Borings B-37, B-45, and B-46, surface materials consisted of 8 to 18 inches of gravel (crushed stone).
- Existing fill was encountered below surface materials in nine (9) borings and generally consisted of silty clay with trace to some crushed stone, crushed asphalt, and organics which extended to depths of approximately 0.5 to greater than 8.5 feet below existing grades in our boring locations. In Boring B-37, fill extended to refusal (possible boulder) at approximately 8.5 feet below existing grades. In Boring B-53, fill extended to boring termination at 5.5 feet below existing grade.
- Fill or surface materials were underlain by native soils. In forty-three (43) borings, native soil consisted of brown to tan to orange brown, low to moderate plasticity, soft to hard, dry to very moist, silty LEAN CLAY with trace to little black oxide nodules. In seven (7) borings, lean clay was extended to refusal or boring termination.
- In forty-eight (48) borings, surface materials, fill, or lean clay were underlain by tan to orange brown with gray mottling, high plasticity, stiff to hard, dry to very moist, silty FAT CLAY with trace to little black oxide nodules which extended to refusal or boring termination.
- In forty-seven (47) borings, refusal was encountered between approximately 1.9 and 11.6 feet below existing grades. Refusal was not encountered prior to boring termination at approximately 8 or 5.5 feet below existing grades at the remainder of borings.
- Refusal materials were cored in four (4) borings and were consisted of light to medium gray to yellow gray, completely weathered to unweathered, thin to massive bedded, soft to hard limestone with interbedded shale in two borings.
- Groundwater was encountered in Boring B-21 in soil-rock interface at approximately 4.5 feet below existing grades. Groundwater was not encountered in the remainder of borings at the time of drilling.

GEOTECHNICAL CONCERNS:

- Shallow Refusal
- Existing UtilitiesPlastic Clays
- Deep Fills
 Existing Fill/Possible Fill
 - Plastic clays
 Pond and Creek
- Existing Fill/Possible Fill
 Existing Constructions
- Agricultural Use
- Existing Pavements
 Trees

DESIGN & CONSTRUCTION RECOMMENDATIONS:

 The proposed buildings may be supported on conventional shallow foundations bearing on stiff or stronger undisturbed inorganic clay, structural fill as defined in this report, flowable fill, lean concrete, or competent bedrock. ECS does not recommend foundations bearing in or within the existing undocumented fill materials. The following net allowable design bearing pressures may be used in foundation design:

- Degradable Soils
- Reuse of On-Site Soils
- Subgrade Improvement
- Weather Considerations

- 2,000 psf for continuous wall foundations bearing on soil.
- 2,400 psf for isolated column foundations bearing on soil.
- 5,000 psf for foundations bearing on competent rock.
- Soil bearing foundations are expected to be dominant. Individual foundations must not bear on soil and rock simultaneously unless they are specifically designed to accommodate the stress concentrations associated with variable bearing conditions (e.g., use of grade beams).
- Existing fill and below grade structures and utilities in the proposed foundation areas should be removed in their entirety. Most of the existing fill encountered did not appear to be adequately compacted. In planned floor slab and pavement areas, existing fill and below grade structures and utilities may be left in-place provided they are 2 feet or more below finished grades, the area is determined to be adequate via proofrolling in the presence of an ECS representative at the time of construction, and the owner is willing to accept the associated risks. If abandoned utilities are left in-place in floor slab and pavement areas, then the abandoned utilities should be grouted full.
- Floors may be designed as slabs-on-grade with a subgrade modulus of 100 pci.
 A site class of "C" may be used in seismic design per the 2018 Kentucky Building Code.
- Foundation excavations and floor and pavement subgrades should be evaluated by an ECS representative during construction to confirm that encountered conditions are consistent with the findings of this exploration.

This summary should not be separated from the entire text of the report with the complete qualifications and considerations mentioned herein. Details of our conclusions and recommendations are discussed in the report text. Findings and recommendations in this report are based on an assumed finish floor elevation. As such, ECS should be contacted to provide appropriate values and recommendations for changes to the assumed elevations.

1.0 INTRODUCTION

1.1 GENERAL

The purpose of this report is to provide the results of our subsurface exploration, engineering analyses, and geotechnical recommendations for the design of foundations, floor slabs, and pavements for the proposed development on Tucker Station Road, Louisville, Kentucky. Also included are geotechnical subgrade preparation and fill placement guidelines. The recommendations developed for this report are based on project information supplied by Mr. Jake Spring of Xebec Realty.

1.2 SCOPE OF SERVICES

Fifty-seven (57) soil test borings were performed at the selected locations in the proposed construction areas. A laboratory testing program was also implemented to characterize the physical and engineering properties of the subsurface soils. This report describes our exploratory and testing procedures, presents our findings and evaluations, and includes the following:

- Summary of the project information provided.
- Description of existing site conditions, reported geology, and encountered subsurface conditions.
- Assessment of general adequacy of the site for the intended use from a geotechnical standpoint.
- Site preparation and structural fill placement recommendations.
- Recommended foundation type(s), design parameters, and construction guidelines.
- Recommended ground floor bearing parameters and construction guidelines.
- Recommended flexible and rigid pavement design parameters and construction guidelines.
- Site class for seismic design based on the boring data and on available data from the vicinity.
- Other identified geotechnical concerns and recommended additional sampling/testing/analysis.

Our services were provided in accordance with our Terms and Conditions of Service included in our Proposal No. 61:P2474, dated September 22, 2021.

2.0 PROJECT INFORMATION

2.1 SITE INFORMATION

SUBJECT	SUMMARY OF EXISTING SITE CONDITIONS		
Site Address	The site is an approximately 108 acres of land on Tucker Station Road in Louisville, Kentucky. For location, refer to Site Location Diagram and Boring Location Plan in Appendix .		
General Description & Topography	The site consists of wooded areas, agricultural fields, several buildings (residential houses) and outbuildings, access roads and driveways, a creek/swale, an existing stockpile of construction debris (mainly crushed asphalt), and an existing pond. The site is undulating but generally sloped downward to the south of the site with a maximum elevation difference of approximately 20 to 30 feet within the proposed building footprints.		
Surface Water Drainage	Surface drainage appeared to be poor to fair.		
Ground Cover	 Topsoil Gravel/crushed stone (in Borings B-37, B-45, and B-46) 		
Existing Utilities	Several underground utilities (including gas, water, electric, communication, etc.) were identified in the proposed construction areas.		

2.2 PROPOSED CONSTRUCTION

SUBJECT	DESIGN INFORMATION / EXPECTATIONS		
Project Description	Four (4) industrial warehouses between approximately 195,000 and 285,000 square feet (a total of approximately 950,000 square feet) with surrounding, loading docks, parking areas, and drive lanes are proposed.		
Usage	Industrial		
Maximum Column Loads	Less than 150 kips (assumed)		
Maximum Wall Loads	Less than 5 kips per linear foot (assumed)		
Finish Floor Elevation	Proposed Building in Lot 1: EL 668 feet (assumed) Proposed Building in Lot 2: EL 674 feet (assumed) Proposed Building in Lot 3: EL 673 feet (assumed) Proposed Building in Lot 3: EL 673 feet (assumed)		
Maximum Cut/Fill	± 15 feet overall site grading for building area (assumed).		
Design Traffic Loads	Light Duty: Daily 18-kip equivalent axle load of 7 (parking areas for cars and light trucks). Heavy Duty: Daily 18-kip equivalent axle load of 75 (drive lanes and entrances for cars, light trucks, and the occasional garbage truck).		

3.0 SITE GEOLOGY

According to the Geologic Map of Jeffersontown Quadrangle, Jefferson County, Kentucky published by the United States Geological Survey (USGS), and information obtained from the Kentucky Geological Survey (KGS) Geologic Information Service website, the majority of the subject site was underlain by "Drakes formation". However, in northwestern portion of the site and along eastern property line, the site was underlain by Osgood & Brassfield Formations.

Site Geology - Underlying Formations ⁽¹⁾			
FORMATION	DESCRIPTION	KARST POTENTIAL ^{2,3}	
Osgood & Brassfield Formations (In northwestern portion and along eastern property line)	 Osgood Shale: a) Shale and dolomite. b) Shale is greenish gray, silty, poorly fissile, dolomitic; weathers to gray flakes or to yellowish gray or grayish yellow clay. c) Dolomite is yellowish gray with reddish or orange mottling (probably a weathered color), fine grained; occurs at base of unit; resembles lowest dolomite bed of the Laurel Dolomite. d) Outcrop areas of the shale are excellent sites for farm ponds. Unit is not resistant to weathering. Brassfield Formation: e) Three types of limestone. Each generally 2 feet or less thick and may be missing at a given locality. f) At top is an orange yellow, medium grained, fossil fragmental limestone. In middle is a medium to dark gray, fine grained, unfossiliferous limestone. At base is a light olive gray, coarse grained, highly fossiliferous limestone. g) Mapped with the Osgood Formation. The karst potential indicated in the adjacent column is for both formations. The Brassfield Formation is susceptible to karst activity. 	Non-karst ⁴	
Drakes Formation (Majority of the site)	 Saluda Dolomite Member: a) Limestone and shale. b) Limestone is light to dark gray, very fine to coarse grained. c) Shale is grayish black, carbonaceous, calcareous, and imperfectly fissile. Bardstown Member: d) LIMESTONE and SHALE. e) Limestone is greenish gray or olive gray, muddy, shaly weathering. f) Shale makes up a small percentage of the unit and is generally indistinguishable from the muddy limestone. g) Basal contact commonly well exposed. Rowland Member: h) LIMESTONE and SHALE. i) Limestone is light gray, olive gray or greenish gray, weathers yellowish gray. Silty and argillaceous, fine to medium grained, slightly dolomitic. j) Shale is olive gray, calcareous, silty and clayey, occurring as partings and thin beds. k) Muddy limestone and shale are more abundant in lower 10 feet and make up about 20 percent of the unit. 	Low⁴	

Notes:

(1) Source: Geologic Map of the Jeffersontown Quadrangle, Jefferson County, Kentucky published by the United States Geological Survey, and information obtained from the KGS Geologic Map Information Service website.

(2) Karst is topography commonly formed over limestone or dolomite and characterized by sinkholes, irregular rock conditions, underground drainage, springs, and caves.

(3) The karst potential level is based on the tendency for the site to develop or have karst features and is not necessarily indicative of the actual presence or absence of existing karst activity at the site.

(4) According to the KGS Potential Classification definitions, formations designated with "non-karst" and "low" karst potential are formations where karst feature are rare or absent, and where karst features are poorly developed or absent, respectively.

4.0 FIELD EXPLORATION AND LABORATORY TESTING

4.1 SUBSURFACE CHARACTERIZATION

SUBJECT	SUMMARY OF SUBSURFACE EXPLORATION (1)		
Boring Method	Continuous Flight Auger & Direct Push		
Sampling Method	Standard Penetration Testing (ASTM D-1586); and Rock Coring (ASTM D-2113)		
Number of Borings	 Building 3 – Borings B-25 through B-35 Building 4 – Borings B-36 through B-41 		
Boring Locations	 Pavements and Drives – Borings B-42 through B-57 Refer to Boring Location Plan in the Appendix for specific locations 		
Boring Depths	Refer to Boring Records in the Appendix		
Logging Method	Full-time presence of an ECS engineer to observe, manage, and document the drilling, sampling and testing results, and encountered conditions. Water level measurement obtained in boreholes during drilling.		
Groundwater	Groundwater was encountered in Boring B-21 in soil-rock interface at approximately 4.5 feet below existing grades. Groundwater was not encountered in the remainder of borings at the time of drilling.		
Refusal ⁽²⁾ In forty-seven (47) borings, refusal was encountered between approximately 11.6 feet below existing grades. Refusal was not encountered prior to termination at approximately 8 or 5.5 feet below existing grades at the remain borings.			

Detailed descriptions of the exploration methods are listed in the Field Procedures section of the Appendix.
 Refusal is the term applied to material that cannot be penetrated with drilling tools or has a standard penetration resistance exceeding 50 blows per 6-inch increment or 10 blows with little to no penetration of the splitspoon. Refusal may be encountered on continuous bedrock, discontinuous floaters, cemented soil, weathered rock, buried construction debris, buried structures, or other hard subsurface materials.

The following sections provide generalized characterizations of the soil strata. Please refer to the **Boring Records** and **Boring Composite(s)** in the **Appendix** for detail at specific boring locations.

APPROXIMATE DEPTH (FT)	STRATUM	DESCRIPTION	N-VALUES BLOWS PER FOOT (BPF) ²
0-1.8	I	TOPSOIL – Approximately 1 to 21 inches. GRAVEL – Approximately 8 to 18 inches (Borings B-37, B-45, and B-46).	N/A
0.1 - 8.5	Ш	FILL/POSSIBLE FILL – Brown, tan brown, orange brown, gray, low to high plasticity, dry to moist, silty CLAY with trace to some crushed stone, crushed asphalt, and organics.	4 to 50+
0.2 - 6.8	B LOW TO MODERATE PLASTICITY CLAY (CL) – Brown, tan to orange brown, low to moderate plasticity, soft to hard, dry to very moist, silty LEAN CLAY with trace to little black oxide nodules.		2 to 21
0.3 - 11.6	0.3 – 11.6IVHIGH PLASTICITY CLAY (CH) – Tan to orange brown with gray mottling, high plasticity, stiff to hard, dry to very moist, silty FAT CLAY with trace to little black oxide nodules.		5 to 38

APPROXIMATE DEPTH (FT)	STRATUM	DESCRIPTION	N-VALUES BLOWS PER FOOT (BPF) ²
7.0 – 22.0	V	LIMESTONE – light to medium gray to yellow gray, completely weathered to unweathered, thin to massive bedded, soft to hard (with interbedded shale in two borings) (Rock Core Borings B-9, B-14, B-32, and B-41)	N/A

Notes:

- This summary is generalized and does not describe the actual conditions in each boring. These zones also may not occur at each location. Depths are approximate. Detailed descriptions of the encountered materials are listed on the Boring Records in the Appendix.
- (2) BPF Blows per Foot

4.2 LABORATORY TEST SUMMARY

Laboratory testing was performed on selected samples obtained during our field exploration operations. Classification and index property tests were performed. The laboratory testing program included:

- Natural Moisture Content
- Atterberg Limits

Each sample was visually classified on the basis of texture and plasticity in accordance with ASTM D2488 Standard Practice for Description and Identification of Soils (Visual-Manual Procedures), including Unified Soil Classification System (USCS) classification symbols, and ASTM D2487 Standard Practice for Classification for Engineering Purposes. After classification, the samples were grouped in the major zones noted on the **Boring Records** in the **Appendix**. The group symbols for each soil type are indicated in parentheses along with the soil descriptions. The stratification lines between strata on the logs are approximate; in situ, the transitions may be gradual.

	SUMMARY OF LABORATORY TEST RESULTS ^{(1), (2)}				
STRATUM	MOISTURE CONTENT (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	UNIFIED SOIL CLASSIFICATION
II	13.7 – 34.8	-	_	-	-
III	11.7 – 34.5	43, 36	24, 21	19, 15	CL
IV	12.3 - 36.4	75, 88, 81, 69, 79, 79, 63	34, 38, 28, 26, 24, 26, 30	41, 50, 53, 43, 55, 53, 33	СН

Notes:

(1) A more detailed summary of the laboratory test results is included on the **Boring Records** in the **Appendix**. Detailed descriptions of the laboratory test methods are listed in the **Laboratory Procedures** section of the **Appendix**.

(2) This table only summarizes the laboratory test results conducted on samples obtained from the recent exploration.

5.0 GEOTECHNICAL CONCERNS

Analysis of the provided project information, observed site conditions, encountered subsurface conditions, and our experience with similar projects, revealed the following important geotechnical considerations. These considerations must be properly addressed in planning, budgeting, design, and construction phases to reduce impacts on construction cost, completion schedule, performance of the building and site improvements, and long-term maintenance of the proposed construction. Our recommendations for addressing these concerns are provided in subsequent sections of this report.

5.1 SHALLOW REFUSAL

- Auger and/or direct push refusal was encountered approximately 1.9 to 11.6 feet below existing grades.
- Based on our assumed FFEs, rock will likely be anticipated at some foundation bearing depths, but soil bearing conditions should predominate throughout the planned foundation areas.
- The presence of refusal above planned foundation, slab, or utility elevations can increase site development costs and slow construction, especially if the cost of excavation methods is not considered in planning and design.
- Foundation design should accommodate the different materials that will be encountered at the foundation depths.
- It is possible that the depth to rock in unexplored areas may vary significantly from the depths indicated by the test borings.
- Removal of most of the on-site refusal material, if necessary, with conventional excavation equipment is not expected to be effective. The competent rock on-site requires special rock removal equipment (e.g., hoeram, blasting, etc.) for efficient excavation.
- The difficulty of removal will be affected by the methodology used, the experience of the operator, and the type of equipment used.
- Greater than normal differential settlement likely will occur if foundations are supported on both rock and soil simultaneously. Alternatives to address this concern are included in **Section 6.6**.

5.2 DEEP FILLS

- Deep fills are considered those more than 10 feet. As fill depths exceed 10 feet, settlement and differential support issues become more of a concern.
- In general, we would anticipate that properly placed and compacted clay fill will consolidate 1 to 2 percent of the height of the fill, which for 10 feet of fill, translates to approximately 1 to 2 ½ inches of settlement associated exclusively from consolidation of the new fill under its own weight.
- While much of this settlement would occur during or shortly after placement, as fills get deeper, the settlement periods lengthens so that some settlement would occur well after placement and could damage overlying construction.
- In addition to the settlement of the new fill, the underlying residual soils also will consolidate under the weight of the new fill. This settlement will increase as both the height of the new fill and the compressibility of the underlying residual soil increases.

- For the anticipated depth of deep fills (generally in the range of 10 to 15 feet), the anticipated settlement of the residual soils under the weight of new deep fills likely would be less than 1 inch.
- Settlement rates can be accelerated by filling above planned grade to surcharge the area.
- Flexible utility connections can be used to accommodate expected differential settlement.
- The concerns associated with deep fills can be reduced by following the fill placement recommendations provided in subsequent sections of this report.

5.3 EXISTING FILL/POSSIBLE FILL

- Existing uncontrolled fill was encountered in several borings. The fill materials encountered appeared to have not been placed in a controlled manner or with adequate compaction effort.
- The existing fill (possible fill) should be considered uncontrolled fill since no records are available documenting the material quality or content. The unknown quality, consistency, and behavior characteristics of uncontrolled fill creates concerns for the behavior of overlying construction.
- Potential problems for the proposed construction created by the presence of the existing uncontrolled fill include larger than normal total and differential settlements, collapse of buried objects, and poor bearing support. The manifestation of these problems can cause poor foundation, slab, and pavement performance.
- Because of the unacceptably high risks associated with uncontrolled fill in foundation areas, support of new foundations in or over uncontrolled fill is not recommended.
- In some cases, existing fill could be left in place in new floor slab and pavement areas if the owner is willing to accept the associated risk, including, but not limited to greater than normal distress and future repair.

5.4 EXISTING CONSTRUCTION

- The planned construction areas included several existing buildings which will be demolished.
- The buried (below grade) components associated with the existing structures (e.g., foundations, utilities, etc.) can cause new construction to behave poorly for many reasons, including stress concentrations resulting from point loading and poor support caused by old backfill.
- Cosmetic and structural damage to the overlying construction can result if the existing building components are not properly addressed during construction.
- Care should be exercised during demolition to reduce the amount of area disturbed during removal activities (e.g., do not push or pull foundations from the ground because this process commonly disturbs large zones of adjacent soils).
- Backfill should be placed following the recommendations under structural fill section.
- It is important that subgrades are carefully evaluated during construction for poorly compacted backfill associated with buried or removed building components and improved as necessary per recommendations provided by ECS during construction.

5.5 EXISTING PAVEMENTS

• Existing surfaces included asphalt parking areas and driveways.

- Existing pavements should be left in-place as long as possible to act as a construction platform.
- Water is commonly trapped under surface paving. Accordingly, soft, saturated soils may be present in some areas below existing pavement.
- Water seepage into excavations from the existing gravel base and utility backfill should be anticipated.
- Moisture conditioning of soils underlying these surface materials commonly is necessary and should be anticipated for this project.
- In addition, asphalt pavement commonly obscures the presence of soft soils. Some undercutting of soft soils below these surface materials should be anticipated.

5.6 EXISTING UTILITIES

- Future access to existing utilities will be difficult if covered by new construction.
- Existing utilities could be damaged by construction activity or by loads from the new structure.
- If existing or former underground utilities are abandoned and not removed or grouted full, soil may migrate into open voids (e.g., open pipes from utilities), causing subsidence of the overlying construction.
- In addition, existing utility lines, if located within proposed construction areas, may cause the new construction to behave unexpectedly due to the variable support conditions caused by old backfill.
- Furthermore, old backfill along utility lines also may provide inadequate support due to poor compaction. The poor support conditions may result in settlement or distress of the overlying new construction. Based on our experience, existing utility backfill rarely is adequate for support of new foundations.
- In floor slab and pavement areas, the load support characteristics of the backfill along utility lines typically can be assessed with careful proofrolling and subgrade evaluation during construction. Some undercutting and/or bridging of these backfill areas should be anticipated.

5.7 PLASTIC CLAYS

- Highly plastic clays (i.e. plasticity index greater than 30 generally designated as "CH" or FAT CLAYS in the report and on boring logs) were encountered in most borings.
- Highly plastic clays are susceptible to volume changes (shrink/swell problems) with changes in moisture. Accordingly, it is advisable to reduce the potential for moisture changes to the soil because of the shrink/swell concerns and the possible impact on the proposed construction.
- Volume changes associated with the highly plastic clays in the geologic formation underlying the site have the potential to produce building or other improvement damage (e.g., floor heave or subsidence, door/window alignment changes, hardscape movements, and drywall cracking).
- Movement may be cyclic (shrink when dry, swell when wet), continuing to produce building distortions that require increased and regular maintenance or repair.
- Typically, the volume changes are not of the magnitude to result in damage that would impair the structural integrity of buildings.

- Exposure to prolonged wet or dry weather conditions during construction can result in volume changes in bearing and subgrade materials or problems achieving the required compaction levels.
- The risks associated with highly plastic clays are common for the project vicinity and are not unique to the site. Most of the effects of highly plastic clays can be reduced by employing the design and construction recommendations described in subsequent sections of this report.

5.8 POND AND CREEK

- A pond was located in the southwestern portion of the proposed Building 1, and a creek was crossing the center of the site form north to south. Soft, inadequate soils (e.g., organic, saturated deposits) requiring remediation and/or stabilization typically are encountered in and around these areas. In addition, trapped and/or perched groundwater can be encountered within these areas.
- The soft, inadequate soils and groundwater issues may complicate construction and increase site development costs. Both conditions should be anticipated along existing drainage swales and within the pond areas and can be addressed during construction with proper planning and budgeting.
- The impact of pond and creek on site development costs can be reduced by scheduling site work during the drier months of the year.

5.9 AGRICULTURAL USE

- Soft soils, organic soils, poorly drained soils, and old drain tiles commonly are associated with the past agricultural activities.
- The upper zone of agricultural land typically is low in density and high in moisture.
- The past agricultural activities may necessitate moisture conditioning, undercutting and/or recompaction of the existing surface soils if exposed at final grades or if fill is to be placed over them, especially if construction occurs during the wetter parts of the year.
- Pockets of soils with a high organic matter (if encountered below the predominant topsoil depths) must be removed.
- Old drain tiles commonly have water trapped in them and often are surrounded by soft, organic soils.
- When drain tiles are damaged during construction, the release of the trapped water can cause problems (e.g., saturation of subgrade soils or the release of water in foundation or utility excavations). These conditions, if they occur, typically are addressed during construction based on the specifics of the individual situation.
- These conditions should be anticipated and included in site preparation planning and budgeting and construction scheduling.
- The impact of past agricultural activities on-site can be reduced by scheduling site work during the drier months of the year.

5.10 TREES

- Mature trees were located within the boundaries of the proposed buildings.
- Organic matter, roots, topsoil, and inadequate soils are associated with trees and heavy vegetative growth.

- Structural problems can result if trees and root balls are not properly removed and backfilled or if topsoil depths are not removed during the earthwork operations.
- Fill material that contains significant roots (i.e., more than 3 percent organics as determined by loss-on-ignition testing) is not adequate for use as controlled fill.
- It is important to note that the topsoil depths reported for this exploration were based on measurements in specific small-diameter samples, which were representative of that location but may not have been representative of each condition or predominant conditions.
- To efficiently remove extensive or pervasive root systems associated with "localized" heavily vegetated areas (e.g., pockets of trees or heavily overgrown areas) and to create a subgrade that drains, it is sometimes necessary to remove topsoil to a consistent depth over an area that exceeds the specific topsoil depths in localized areas (e.g., may strip 12 inches in an area even though the topsoil depths varied from 4 to 12 inches).
- Stripping more than the reported topsoil depths should be expected in some areas, especially areas with current or past heavy vegetation growth or trees.

5.11 DEGRADABLE SOILS

- Most of the soils on-site are susceptible to degradation. Degradable soils readily lose strength, become soft, and "pump" when subjected to construction equipment, especially under wet conditions.
- Undercutting and/or stabilization of soft clay soils could have a cost impact on the project, especially if not properly addressed in the project documents (e.g., definition of what is inadequate and the responsibility for maintenance of these soils once stabilized) or if not properly addressed during construction (e.g., subjected to repeated construction traffic with no protection).

5.12 REUSE OF ON-SITE SOILS

- In general, most of the on-site soils appeared adequate for reuse as structural fill provided the soils are moisture conditioned to appropriate moisture contents for compaction.
- Existing fill may be considered for reuse provided no inadequate materials are present. Sorting to remove inadequate (e.g., organics, remnant topsoil, remnant construction debris, etc.) or oversized material from the existing fill should be expected prior to reuse.
- Some wetting, drying, mixing or chemical treatment of the soils may be necessary to obtain workable moisture contents for the on-site soils, especially during wetter times of the year.
- Reuse of the on-site soils will be subject to the weather considerations described subsequently.

5.13 SUBGRADE IMPROVEMENT

- Most borings encountered soft, weak soils in the upper approximate 2 to 2.5 feet below existing grades.
- Localized improvements will likely be needed in some areas, especially if construction occurs during the wetter/cooler periods of the year.
- The required extent of improvement will depend to a large degree on when earthwork operations take place as well as on how the earthwork contractor prepares the site. The level of improvement likely will increase if:
 - Construction traffic is concentrated along localized soft or poor subgrade routes.

- Earthwork occurs during cool, wet periods (typically November through May).
- Provided construction occurs during the drier time of the year, it would be our expectation that much of the improvement could be achieved by scarifying, drying and recompacting the soils. If construction occurs during the wetter periods of the year, more aggressive treatment would likely be required (i.e., removal and replacement or lime drying).
- Subgrade improvement alternatives, if required, include but are not limited to:
 - Scarification, drying, and recompaction of surface materials.
 - Removal of inadequate materials and replacement with structural fill.
 - Bridging with a thick lift of limestone aggregate.
 - Placement of a geosynthetic or geo-grid in combination with granular fill.
 - Chemical stabilization and/or modification (e.g., kiln dust, lime, or Portland cement).
- The type of subgrade improvement chosen should take weather limitations, or other limitations unique to each method, into consideration.

5.14 WEATHER CONSIDERATIONS

- Conducting site work during periods of cool and/or wet weather (typically November to May) can be problematic for sites in the project region.
- Proper compaction of clay fill generally is very difficult to achieve during periods of cool and/or wet weather. Some drying, mixing, or chemical treatment of the soils would be necessary to obtain workable moisture contents for the on-site soils or proposed borrow materials if placed during the cool, wet seasons.
- If compaction of clay fill takes place under wet weather conditions, increased earthwork costs, an extended construction schedule, and soil improvement (likely chemical stabilization) likely would be required. In addition, reuse of the site soils may be severely limited.
- Surface soils tend to be softer during wet weather conditions due to the excess moisture in the near surface soils.
- Weather-softened surface soils tend to result in more undercutting and/or stabilization than would be required during dry weather conditions, which increases site development costs.
- Project specifications should include definitions and require contractors to provide unit rates for subgrade stabilization, removal of inadequate soils, and replacement of inadequate soils with structural fill appropriate for use during the anticipated construction season.

6.0 SITE CONSTRUCTION RECOMMENDATIONS

6.1 PLANNING

- Adjust project plans, specifications, schedules and budgets to incorporate the issues discussed in **Section 5.0** and the recommendations provided herein.
- It will be critical that the planning of earthwork operations is carefully considered and executed given the presence of degradable soils.
- Findings and recommendations in this report were based on assumed finish floor elevations. As such, ECS should be contacted to provide appropriate values and recommendations for changes to the assumed elevations.

6.2 SUBGRADE PREPARATION

- Localized improvements will likely be needed in some areas, especially if construction occurs during the wetter/cooler periods of the year.
- The depth and extent of improvement required will be dependent on the time of year of construction, the weather preceding site work, and the site work techniques employed.
- The following subsections describe our general recommendations for preparing the site subgrade prior to fill placement operations.

Stripping and Grubbing:

- Materials required to be stripped:
 - Topsoil, asphalt pavements, vegetation, large root zones, organic material, and excessively wet, desiccated, frozen, contaminated, existing fill (especially with shale content), or otherwise inadequate materials.
- Minimum extent of stripping:
 - 10 feet beyond the building limits.
 - 5 feet beyond the pavement limits.
- ECS should observe and document that topsoil and poor surficial materials have been removed prior to the placement of structural fill or construction of structures.
- Stripped material not meeting structural fill requirements should be considered for reuse in landscaped areas only.

Subgrade Evaluation:

- Proofroll the site in the presence of an ECS representative with a pneumatic-tired vehicle (e.g., triaxial dump truck) loaded as recommended by the ECS representative.
- Proofroll subgrades prior to filling or after excavation to grade.
- Proofroll slab and pavement subgrades prior to granular base placement.
- Areas judged by the ECS representative to deflect excessively during proofrolling should be remediated in accordance with ECS recommendations provided at that time.
- Most borings encountered soft, weak soils in the upper approximate 2 to 2.5 feet below existing grades which probably will not pass a proofroll. Therefore, some remediation of soft soils should be anticipated.

• Prepare subgrades with a slight slope to maintain surface drainage.

Other Measures:

- Roll subgrade surfaces smooth if rain is expected.
- Slope final subgrades away from the proposed structure.
- Rough grade subgrades high to allow for removal of degraded soil.
- Remove soil frozen or softened by rain.

6.3 STRUCTURAL FILL

Subgrade Requirements:

• Subgrade proofrolled and required improvements completed.

Fill Material Requirements:

- No shale content.
- No deleterious debris.
- No rock pieces larger than 3 inches.
- Less than 3% organic material (loss on ignition).
- Maximum dry density of at least 100 pcf according to the Standard Proctor compaction method (ASTM D-698), unless specifically reviewed otherwise by ECS.
- Acceptable Unified Soil Classifications (USCS): CL, ML, GW, GM, GC, GP, SW, SP, SM, SC.
- Unacceptable USCS classifications: CH, OL, OH, Pt, MH.
- Evaluated and approved by ECS prior to construction.

Fill Placement Guidelines:

- Minimum compaction:
 - 98 % Standard Proctor maximum dry density (ASTM D-698).
- Moisture Content:
 - Within 2 % of optimum (ASTM D-698) if plasticity index less than 30.
- Maximum loose lift thickness: 8 inches.
- Compaction test frequency:
 - One test per lift for each 5,000 square feet of fill placed.
 - Minimum of 3 tests per lift.
- Bench new fill into existing slopes or sidewalls of deep excavations in 1-foot steps or as recommended by ECS at the time of construction.
- Compact and test each lift prior to placing additional lifts.
- Scarify smoothed fill surfaces prior to placing the next lift.
- Maintain positive surface drainage on fill surfaces during placement to avoid ponding of water.
- Roll fill surfaces smooth if rain is expected.
- Rough grade high to allow for removal of degraded surface soils if fill will be exposed to adverse weather conditions.

• Do not place fill on a frozen subgrade. At a minimum, remove frozen material, or allow to thaw and then recompact.

6.4 EXISTING FILL/POSSIBLE FILL

General Comments:

- The recommendations contained in this report assume that the existing fill is uncontrolled fill.
- Structural fill should be placed and compacted in accordance with the recommendations provided in this report.

Foundation Areas:

- Foundations must not bear in or over existing fill.
- Foundations must penetrate existing fill and bear on stiff or stronger undisturbed inorganic clay, structural fill as defined in this report, flowable fill, or lean concrete.

Floor Slabs and Pavements:

- If existing fill is left in-place in floor slab and pavement areas and the owner is willing to accept he associated risks, the risks associated with the existing fill in floor slab and pavement areas can be reduced by implementing the following recommendations:
 - Visual observation and proofrolling evaluation of the subgrade by an ECS representative at the time of construction.
 - Improvement of the subgrade where and how recommended by ECS based on the results of proofrolling and observations.
- If the risks associated with the existing fill, as described in a previous section, are not acceptable, existing fill should be removed and replaced with controlled fill.

6.5 EXISTING CONSTRUCTIONS

General Comments:

- Recommendations to address existing constructions can be affected by many factors, including factors that are not obvious until construction (e.g., removal of some features creates more potential problems and risks than leaving them in-place).
- As such, the recommendations provided below should be considered general guidelines. If modification to the recommendations provided below is needed, ECS should be contacted for guidance.

Building Components:

- Demolish and remove existing construction within the proposed foundation areas from existing or former construction in the area. Be sure to remove existing foundations, slabs, possible below grade walls, pavements, and buried utilities.
- Backfill the resulting excavations with properly placed and compacted fill that is keyed into the native soil in one-foot steps to provide a gradual transition in support conditions.
- It may be feasible to leave below grade structures in-place in proposed floor slab and pavement areas provided the below grade structures are removed to 2 feet below the

subgrade, the surrounding soils are determined to be unyielding under proofrolling, below grade structures do not conflict with new construction, and the owner is willing to accept the associated risks.

- Old floors or pavements, if encountered, must be broken up or penetrated at regular intervals to promote water drainage or be removed if in new foundation areas.
- The areas where existing construction was located need to be carefully proofrolled in the presence of an ECS representative.
- In addition to proofrolling, very careful earthwork evaluations must be conducted during construction to detect the presence and/or potential anomalies associated with the existing construction.

Utilities:

- Utilities should be relocated as necessary.
- Existing utilities within the proposed building area should be removed in their entirety (including line and associated backfill) unless the risk of damage to the proposed structure has been understood and accepted by the owner. The resulting excavation should then be backfilled in accordance with the recommendations in this report (including benching side slopes and proper compaction).
- Provided the risks associated with leaving utilities in-place are acceptable to the owner, abandoned lines should be grouted full.
- Needed improvements to poor backfill conditions should be identified during construction via proofrolling and surface probing by an ECS representative and remediated in accordance with the recommendations provided by ECS at the time of construction.

6.6 SHALLOW ROCK

- Auger and/or direct push refusal was encountered in the borings at approximately 1.9 to 11.6 feet below existing grades.
- Greater than normal differential settlement likely will occur if foundations are supported on both rock and soil simultaneously. Alternatives to address this concern include:
 - Adjust the floor elevation and/or building location to avoid this condition.
 - Remove rock and backfill with compacted clay or manufactured sand fill where necessary, so that foundations bear on at least 24 inches of approved native soil or controlled fill.
 - Support the building on isolated column foundations tied together with grade beams to reduce the effects of differential settlement. Isolated columns may bear entirely on rock or on soil but not both simultaneously. Adjacent columns may bear entirely on rock or soil.
 - Divide the building into sections that are entirely support on rock or on soil. Design for approximately 1 inch of differential settlement between sections.
- The method used to remove the on-site rock, if necessary, should be selected by the contractor. Removal of the on-site rock with conventional excavation equipment is not expected to be effective. The competent rock on-site requires special rock removal equipment (e.g., blasting, hoe-ram, etc.) for efficient excavation.

6.7 PLASTIC CLAY

- The measures provided below will significantly reduce, but not eliminate, the likelihood the proposed construction will be impacted by the presence of plastic clays:
 - Test the moisture content of subgrade soils. Adjust soil moisture if the results fall outside the range of optimum to plus 3% above optimum.
 - Roof drains and surface drainage should not discharge or be directed to the ground surface within 20 feet of the proposed structures, unless the surface is impervious (such as concrete or pavement), to reduce moisture changes of the foundation soils.
 - Proper drainage should be provided around the proposed construction (e.g., slope the surface away from the building).
- If the risks associated with the plastic clays are not acceptable, then:
 - Do not place plastic clay fills within 2 feet of the planned finish subgrades (building and pavement).
 - Undisturbed plastic clays within 2 feet of planned finish subgrades and foundation bearing elevations are removed and replaced with low to moderate plasticity clay fill soils.

7.0 DESIGN RECOMMENDATIONS

7.1 SHALLOW FOUNDATIONS

General Comments:

- The proposed buildings may be supported on conventional shallow foundations.
- Foundations must bear on stiff or better undisturbed clay, Structural Fill, flowable fill, lean concrete, or competent bedrock. However, soil bearing foundations are expected to be dominant.
- Foundation bearing conditions should be carefully evaluated by ECS during construction.

Variable Bearing Conditions:

- Individual foundations must not bear on soil and rock simultaneously unless they are specifically designed to accommodate the stress concentrations associated with variable bearing conditions (e.g., use of grade beams).
- Individual foundations should bear entirely on soil or entirely on rock (i.e., one isolated column foundation may bear on soil while an adjacent one may bear on rock, but each isolated foundation may not bear on soil and rock simultaneously).
- To address the concerns associated with variable bearing concerns, a minimum 2-foot soil cushion should be present below soil-bearing foundations. This may require the removal of some rock to construct the soil cushion.
- The soil cushion may consist of clay or sand, but not gravel. The cushion should be placed and compacted in accordance with the "Structural Fill" recommendations provided in this report.

Foundation Design Recommendations:

FOUNDATION DESIGN RECOMMENDATIONS					
DESIGN	SOIL BI	ARING	ROCK BEARING		
PARAMETER	CONTINUOUS WALL FOUNDATIONS	ISOLATED COLUMN FOUNDATIONS	CONTINUOUS WALL FOUNDATIONS	ISOLATED COLUMN FOUNDATIONS	
Net Allowable Bearing Pressure ⁽¹⁾	2,000 psf	2,400 psf	5,000 psf	5,000 psf	
Acceptable Bearing Material	Stiff Undisturbed Native Soils, Structural Fill, Flowable Fill, or Lean Concrete.	Stiff Undisturbed Native Soils, Structural Fill, Flowable Fill, or Lean Concrete.	Competent Bedrock: Relatively Unweathered Bedrock.	Competent Bedrock: Relatively Unweathered Bedrock.	
Minimum Width	18 inches	24 inches	18 inches	24 inches	
Depth of Foundations Subject to Freezing (Below slab or finished grade) ⁽²⁾	30 inches	30 inches	30 inches	30 inches	
Depth Foundations Protected from Freezing	12 inches	12 inches	12 inches	12 inches	

• The design of the foundation should utilize the following parameters:

	FOUNDATION DESIGN RECOMMENDATIONS				
DECION	SOIL BEARING		ROCK BEARING		
DESIGN PARAMETER	CONTINUOUS WALL FOUNDATIONS	ISOLATED COLUMN FOUNDATIONS	CONTINUOUS WALL FOUNDATIONS	ISOLATED COLUMN FOUNDATIONS	
Estimated Total Settlement ⁽⁴⁾	≤1 inch	≤ 1 inch	Negligible	Negligible	
Estimated Differential Settlement ⁽⁴⁾	≤ ¾ inch along 50 feet	≤ ¾ inch between columns	Negligible	Negligible	

Notes:

- (1) Net allowable bearing pressure is the applied pressure in excess of the surrounding overburden soils above the base of the foundation.
- (2) The 2018 Kentucky Building Code requires a minimum foundation embedment depth of 24 inches for foundations subject to freezing in Jefferson County. However, a minimum embedment of 30 inches is common for commercial development in the project region.
- (3) The recommended net allowable bearing pressures may be increased 33 percent for transient loading.
- (4) The estimated settlement potential is based on the following: empirical guidelines for the project material types and consistencies; the assumption that ECS will observe and test each foundation excavation during construction; and the provided project information. Actual settlements will depend, in part, on site preparation and conditions at each foundation location.

PARAMETERS FOR FOUNDATION LATERAL RESISTANCE	ESTIMATED VALUE ⁽¹⁾
Coefficient of Active Earth Pressure $(K_o)^{(2)}$	0.41
Coefficient of At-Rest Earth Pressure (K _o) ⁽²⁾	0.58
Coefficient of Passive Earth Pressure (K _p) ⁽²⁾	2.46
Moist Unit Weight of Soil (γ)	125 pcf
Base Shear Adhesion [Concrete on Undisturbed Clay]	400 psf
Coefficient of Friction [Concrete on Clay] (μ)	0.30
Coefficient of Friction [Concrete on Rock] (μ)	0.50

Notes:

- (1) These design parameters do not include factors of safety. Appropriate factors of safety should be included in the designs.
- (2) Provided earth pressure coefficients are based on an assumed internal angle of friction (ϕ) of 25 degrees for clay.
 - Desiccation or disturbance may result in soil voids or cracks adjacent to foundations, reducing passive and uplift resistance. As a result, for these calculations, the upper 2.5 feet of soils should be neglected for passive resistance.
 - Ignore passive earth pressure if the soil against the sides of the foundations may not be present during the life of the structure (e.g., the soil could be excavated or be subject to erosion).

Construction Guidelines:

- The bearing conditions of each foundation should be evaluated by ECS at the time of construction to confirm the presence of adequate bearing soils and to provide recommendations for the remediation of poor soils, if present. This evaluation should be performed before the reinforcing steel is placed in the excavations.
- Concrete should be placed the same day the foundations are excavated to reduce degradation of the bearing surface due to exposure. Alternatively, a "mud mat" of lean concrete should be placed to protect the bearing surface.

• Disturbed, degraded or loose material should be removed from the excavation bottoms prior to concrete placement.

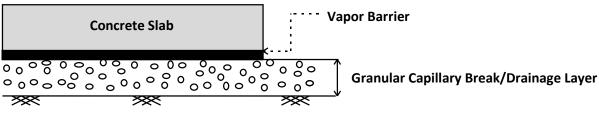
7.2 FLOOR SLABS

Recommended Slab Type:

• Grade supported floor slabs

Floor Subgrade Recommendations:

- Prepare subgrade in accordance with recommendations contained within this report.
- Subgrade proofrolled by an ECS representative and required improvements completed.
- Subgrade modulus for slab design: 100 pci.
- Place a minimum of 4 inches of well-graded crushed stone or angular sand base.
- Compact base material in accordance with the structural fill recommendations provided previously.
- Unless specifically approved otherwise, do not support floor slabs directly over opengraded coarse aggregate to avoid loss of concrete, increased concrete cracking during drying shrinkage, and puncture of the vapor barrier. If coarse aggregate is used as a drainage base, cap the coarse aggregate with a 2-inch (minimum) layer of well-graded aggregate (e.g., KYTC DGA).
- The following graphic depicts our soil-supported slab recommendations:



Compacted Subgrade

Notes:

- (1) Drainage layer should consist of a minimum of 4 inches of well graded crushed stone or angular sand or open-graded coarse gravel. However, if open graded sone is selected then a minimum 2-inch layer of coarse aggregate with fines (e.g., KYTC DGA) should be used to cap the open graded stone.
- (2) Subgrade compacted to 98% maximum dry density per ASTM D698.

Construction Guidelines:

- If a vapor barrier will be used, an adequate concrete design mix, placement, finishing, and curing techniques should be employed to reduce the potential for differential slab shrinkage, cracking, and curling.
- Special care must be taken to avoid puncturing the vapor barrier during construction. We recommend utilizing the ACI 302 guidelines for placement of the vapor barrier, manufactured sand layer, and concrete as a function of the construction sequence.
- Drying shrinkage and concrete curing methods frequently causes floor slab cracks. Control joints and saw cuts should be installed in accordance with ACI guidelines to control cracking.

- Slab joints should be doweled or keyed to allow rotation of the slab sections without localized vertical displacement.
- Penetrations of the floor slab by fixed objects, such as drains or piping, restrict shrinkage movement and must be isolated to reduce cracking potential.
- Slab-on-grade floor should be structurally isolated from foundation supported walls.
- Backfill along foundation excavations should be carefully controlled to reduce differential slab settlement.

7.3 SEISMIC DESIGN CONSIDERATIONS

- The 2018 Kentucky Building Code (KBC) requires site classification for seismic design based on the upper 100 feet of a soil profile. At least two methods are utilized in classifying sites, namely the shear wave velocity (vs) method and the Standard Penetration Resistance (N-value) method. The second method (N-value) was used in classifying this site.
- Based upon our interpretation of the subsurface conditions, the appropriate Seismic Site Classification is **"C"** as shown in the preceding table.

	SEISMIC SITE CLASSIFICATION					
Site Class	Soil Profile Name	Shear Wave Velocity, Vs, (ft./s)	N value (bpf)			
Α	Hard Rock	Vs > 5,000 fps	N/A			
В	Rock	2,500 < Vs ≤ 5,000 fps	N/A			
С	Very dense soil and soft rock	1,200 < Vs ≤ 2,500 fps	>50			
D	Stiff Soil Profile	600 ≤ Vs ≤ 1,200 fps	15 to 50			
E	Soft Soil Profile	Vs < 600 fps	<15			

Ground Motion Parameters:

In addition to the seismic site classification noted above, ECS has determined the design spectral response acceleration parameters following the International Building Code (IBC) 2015 methodology. The Mapped Reponses were estimated from the OSHPD Seismic Design Map website (<u>http://seismicmaps.org/</u>). The design responses for the short (0.2-sec, S_{DS}) and 1-second period (S_{D1}) are noted at the right end of the following Table:

GROUND MOTION PARAMETERS [IBC 2015 Method]								
Period (sec)	Mapped Spectral Response Accelerations (g)		Values of Site Coefficient for Site Class		Maximum Spectral Response Acceleration Adjusted for Site Class (g)		Design Spectral Response Acceleration (g)	
0.2	Ss	0.192	Fa	1.2	$S_{MS} = F_a S_s$	0.231	S _{DS} =2/3 S _{MS}	0.154
1.0	S ₁ 0.101		F_{v}	1.699	$S_{M1}=F_vS_1$	0.172	S _{D1} =2/3 S _{M1}	0.115

• The Site Class definition should not be confused with the Seismic Design Category designation which the Structural Engineer typically assesses.

7.4 FLEXIBLE PAVEMENT DESIGN

Application:

• Main driving lanes, parking areas or other locations where heavy vehicle or other equipment will not turn on a tight radius or be parked for extended periods of time.

General Comments:

- The pavement sections below are guidelines that may or may not comply with local jurisdictional minimums.
- If the traffic loads, Daily Equivalent 18-kip Axle Loads (DEALs), used in this report differ from the expected traffic loads onsite, ECS should be contacted to modify the pavement design.

FLEXIBLE DESIGN PARAMETERS		
Design Method	AASHTO Guide for Design of Pavement Structures (1993)	
Daily Equivalent 18-KIP Axle Loads	7 (Light Duty) – Car parking areas.	
Dany Equivalent 10-kii Axie Eduus	75 (Heavy Duty) – Semi Parking Areas.	
Design Life	20 Years	
California Bearing Ratio (CBR)	3 (Assumed)	
Reliability	80%	
Terminal Serviceability Index	2.0	

RECOMMENDED FLEXIBLE PAVEMENT SECTIONS ⁽¹⁾								
Pavement Section	Hot Mix Asphalt Wearing Surface	Hot Mix Asphalt Binder or Base	Granular Base Kentucky DGA					
Light Duty	1 inch	2 inches	8 inches					
Heavy Duty	1 inch	4 inches	12 inches					

Notes:

(1) It should be noted that although flexible pavement for the 20-year design period is structurally sound, an asphalt overlay is usually necessary after 7 to 12 years due to normal wear and exposure of the surfacing layer. In general, asphalt pavement should be sealed approximately 3 to 5 years to extend the life of the asphalt.

Subgrade Requirements:

- Prepare subgrade in accordance with recommendations contained within this report.
- Proofroll in the presence of an ECS representative and complete required improvements.
- Pavement subgrades sloped to facilitate drainage.

Drainage Requirements:

- Permit water movement beneath curbs at the subgrade level.
- Design catch basins to include finger drains at the granular base level.

Construction Guidelines

- Pavements should be constructed in accordance with the construction and material guidelines in the most recent edition of the Kentucky Transportation Cabinet's "Standard Specifications for Road and Bridge Construction."
- Granular base should be compacted in accordance with the structural fill recommendations provided in a previous section.
- In-place density, thickness, and gradation tests should be conducted by a ECS representative on the pavement components during construction to confirm compliance with project specifications.

7.5 RIGID PAVEMENT DESIGN

Application:

 Rigid pavements are adequate wherever flexible pavements can be used. Rigid pavements often provide better service for dumpster aprons, entranceways, or other areas where heavy trucks will turn on a tight radius or be parked for extended periods of time.

General Comments:

• The pavement sections below are guidelines that may or may not comply with local jurisdictional minimums.

RIG	RIGID PAVEMENT DESIGN PARAMETERS		
Design Method	ACI Guide for the Design and Construction of Concrete Parking Lots (ACI 330R-08)		
Traffic Category	A (Light Duty): Car parking areas and access lanes C (Heavy Duty): Semi parking areas.		
Design Life	20 Years		
California Bearing Ratio (CRR)	3 (Assumed)		
Effective Subgrade Modulus	100 pci		
Concrete Modulus of Rupture	500 psi		

RECOMMENDED RIGID PAVEMENT SECTIONS						
Pavement Section Portland Cement Concrete Granular Base Kentucky DC						
Light Duty	5 inches	4 inches				
Heavy Duty	7 inches	6 inches				

Subgrade Requirements:

- Prepare subgrade in accordance with recommendations contained within this report.
- Proofroll in the presence of an ECS representative and complete required improvements.
- Pavement subgrades sloped to facilitate drainage.

Drainage Requirements:

- Permit water movement beneath curbs at the subgrade level.
- Design catch basins to include finger drains at the granular base level.

Concrete Recommendations:

- 4,000 pounds per square inch (psi) minimum 28-day compressive strength.
- 4 to 6 percent entrained air.
- Proper joint spacing to control shrinkage cracking.
- Dowels at construction joints to properly transfer loads between pavement sections.
- Control joints where concrete pavement abuts fixed structures or protrusions.

8.0 CLOSING

There are certain limitations inherent to geotechnical explorations and reports. These limitations are discussed below and in the **GBA "Important Information About Your Geotechnical Engineering Report"** in the **Appendix**. They should be fully considered prior to using the recommendations in this report.

Our geotechnical exploration identified the subsurface conditions that existed only at the locations and times that the borings were advanced. Given the natural variable characteristics of soil and rock, conditions may vary over short distances, change with time, or be affected by natural events, such as floods or earthquakes, or by human activity, such as past land use or new construction. As such, the information generated during our geotechnical exploration may not be representative of the entire conditions that may exist on the project site now or in the future. We use our professional judgment to render an opinion about the subsurface conditions that may exist in the areas of the site not specifically tested during our exploration based on our review of available field and laboratory data and our past experience with similar subsurface conditions. However, the subsurface conditions between our borings and in unexplored areas of the site could affect our interpretations. Thus, it is important to retain ECS to provide construction monitoring services based on our involvement in the project, our knowledge about the site, and our knowledge relating to the assumptions and recommendations contained within this report.

The recommendations contained within this report are dependent on many factors, including, but not limited to, the project information provided by others and the specific conditions encountered during our exploration. If the project information contained within this report is incorrect or changed at a later date or if the location or nature of the structures or facility components changes, ECS should be notified and given the chance to assess the impact of the changes. We cannot and do not accept responsibility or liability for problems that occur because we were not given the opportunity to properly assess changes to the project. The recommendations contained in this report must not be considered valid unless our firm reviews such changes and required modifications to our recommendations are verified in writing.

Our recommendations are dependent on several factors including, but not limited to, our review of project drawings and specifications prior to construction and observation of actual conditions during construction, including providing the required Special Inspections. We strongly recommend that ECS be retained to review pertinent portions of the project plans and specifications.

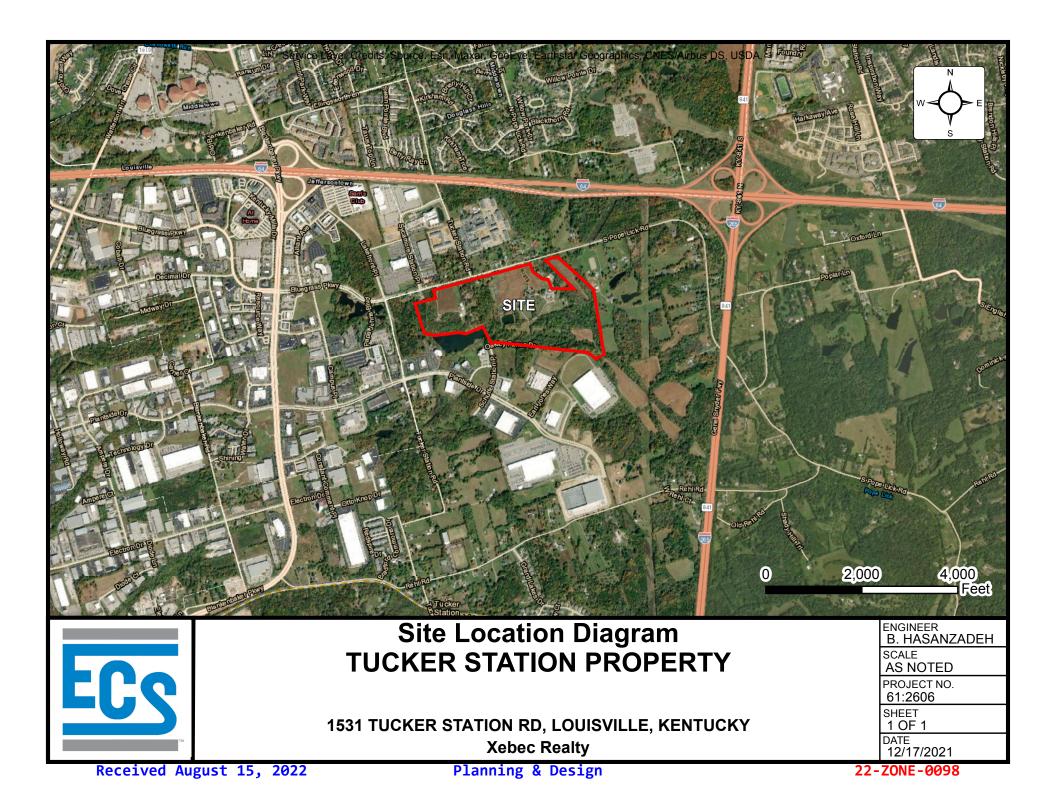
This report should be reproduced in its entirety only. Portions of this report should not be separated and used by others. It should be noted that this report was not prepared for the purpose of bid development and should not be used as such.

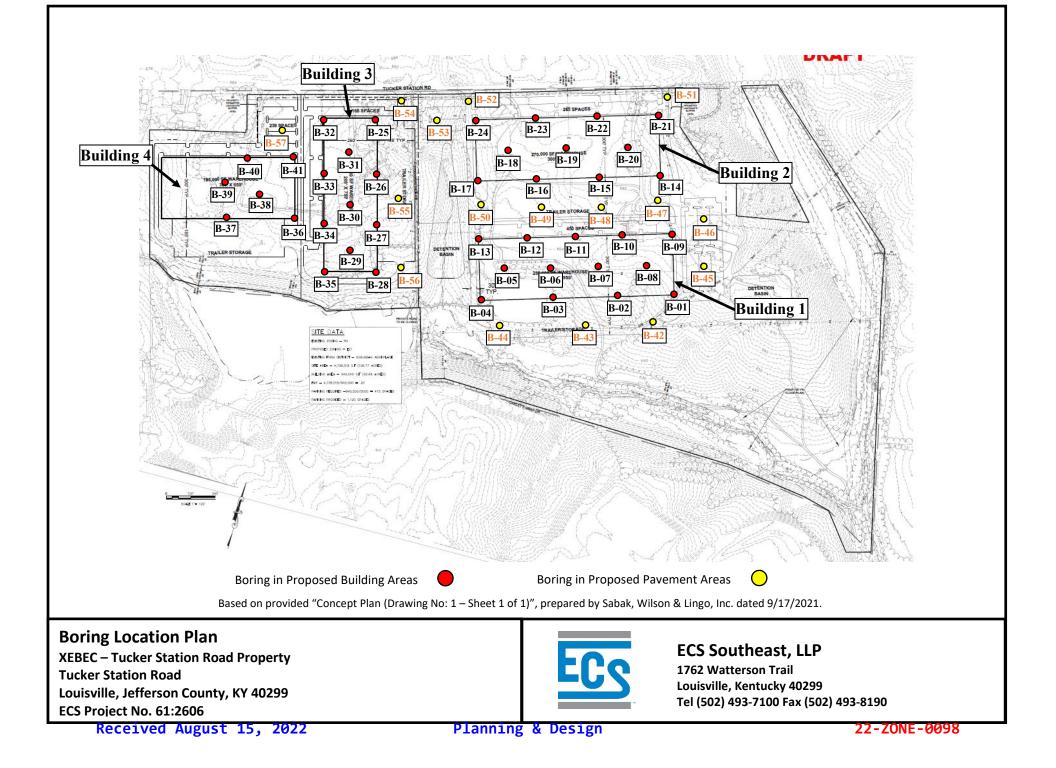
This geotechnical report is unique and was based on client needs and project requirements for the specific project described in this report. As such, no one other than who the report was intended and prepared for should rely on this report or the information contained within the report without first consulting with ECS. This report is not valid for any purpose or project except as described in this report.

This report and our recommendations were prepared using the generally accepted standards of geotechnical engineers practicing in this region. No warranty is express or implied.

APPENDIX

Site Location Diagram Boring Location Plans Soil & Rock Classification Boring Legend Boring Records Boring Composite Field Procedures Laboratory Procedures







ECS Southeast, LLP

SOIL & ROCK CLASSIFICATION

	MAJOR DIVISI	ONS	SYMBOLS	TYPICAL DESCRIPTIONS
004005	GRAVEL Cloge Gravels		GW	Well graded gravels, gravel-sand mixtures, little or no fines
COARSE GRAINED	AND			Poorly graded gravels, gravel-sand mixtures, little or no fines
SOILS	GRAVELLY	Gravels	GM	Silty gravels, gravel-sand-silt mixtures
MORE THAN	SOILS	with fines	GC	Clayey gravels, gravel-sand-clay mixtures
50% OF	SAND		SW	Well graded sands, gravelly sands, little or no fines
MATERIAL IS LARGER	AND	Clean Sands	SP	Poorly graded sands, gravelly sand, little or no fines
THAN NO. 200 SIEVE	SANDY	Sands	SM	Silty sands, sand-silt mixtures
SOILS	with fines	SC	Clayey sands, sand-clay mixtures	
FINE	FINE		ML	Inorganic silts, silty or clayey fine sands or clayey silts with slight plasticity
GRAINED	AND CLAYS less than 50		CL	Inorganic clays of low to moderate plasticity, gravelly clays, sandy clays, silty clays, lean clays
			OL	Organic silts and organic silty clays of low plasticity
MORE THAN 50% OF	SILTS	Liquid Limit areater	MH	Inorganic silts, micaeceous or diatomaceous fine sand or silty soils
MATERIAL IS SMALLER	13		СН	Inorganic clays of high plasticity
THAN NO. 200 SIEVE	CLAYS	Than 50	ОН	Organic clays of moderate to high plasticity, organic silts
HIGHLY ORGANIC SOILS		PT	Peat, humus, swamp soils with high organic contents	

SOIL CONSISTENCY SPT N: Standard Penetration Test N-Value N¹ - Manual Hammer (Rope & Pulley - 60% Efficiency) N² - Automatic Hammer (Free-Fall - 96% Efficiency)

COARSE GRAINED SOILS		FINE GR	AINED SO	DILS	
SPT N ¹	SPT N ²	Relative Density	SPT N ¹	SPT N ²	Field Identification
0-4	0-3	Very loose	0-2	0-1	Very soft – Easily penetrated several inches by fist
4-10	3-6	Loose	3-4	2-3	Soft – Easily penetrated several inches by thumb
10-30	6-19	Medium dense	5-7	3-4	Firm – Can be penetrated several inches by thumb with moderate effort
30-50	19-31	Dense	8-15	5-9	Stiff – Readily indented by thumb but penetrated only with great effort
> 50	> 31	Very dense	16-30	10-19	Very stiff – Readily indented by thumbnail
			> 30	> 19	Hard – Indented with difficulty by thumbnail

SOIL PARTICLE SIZ	ES	
Description	Size Limits	Familiar Example
Boulder	12 inches or more	Larger than basketball
Cobble	3 - 12 inches	Orange to basketball
Coarse gravel	¾ - 3 inches	Grape to orange
Fine gravel	4.75 mm (No. 4 sieve) - ¾ inch	Pea to grape
Coarse sand	2-4.75 mm (No. 10 to 4 sieve)	Rock Salt
Medium sand	0.42-2 mm (No. 40 to 10 sieve)	Table Salt
Fine sand	0.075-0.42 mm (No. 200 to 40 sieve)	Powdered sugar
Silt/Clay/Fines	Less than 0.075 mm (No. 200)	Not visible to naked eye

RELATIVE PROPORT	ONS
Description	Percent
Trace	1-5
Few	5-15
Little	15-30
Some	30-50
Mostly	50-100

ROCK CONTINUITY	
Description	Core Recovery (%)
Incompetent	0-40
Competent	40-70
Fairly Continuous	70-90
Continuous	90-100

ROCK QUALITY DESIGNATION				
Description	RQD (%)			
Very Poor	0-25			
Poor	25-50			
Fair	50-75			
Good	75-90			
Excellent	90-100			

Description	Thickness (in)
Parting	< 0.3
Band	0.3-2.5
Thin Bed	2.5-6.0
Medium bed	6.0-12.0
Thick bed	12.0-36.0
Massive	> 36.0

POCK REDDING

ROCK HARDNESS (Descriptions for rock core samples)

Description	Definition
Very soft	Can be broken with fingers
Soft	Can be scratched with fingernail; only edges can be broken with fingers
Moderately hard	Can be easily scratched with knife; cannot be scratched with fingernail
Hard	Difficult to scratch with knife; hard hammer blow to break specimen
Very hard	Cannot be scratched with knife; several hard hammer blows to break specimen

ROCK WEATHERING (Descriptions for rock core samples)

Description	Definition
Completely	Rock decomposed to soil; rock fabric and structure
	completely destroyed
Highly	Most minerals are decomposed; texture indistinct but
	fabric preserved; strength greatly reduced
Moderately	Discoloration throughout and weaker minerals
	decomposed; texture preserved but strength less than
	unweathered rock
Slightly	Discoloration around open fractures; strength
	preserved
Unweathered	No sign of decomposition

Received August 15, 2022 Planning & Design



ECS Southeast, LLP 1762 Watterson Trail

Louisville, Kentucky 40299

BORING LEGEND

Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
		<u>7, 7, 1</u>	TOPSOIL	1.0								Scale - Proportional distance below the surface.
	-		GRAVEL, crushed stone, (FILL)									Elevation - Vertical distance above or below a benchmark.
_	-		CLAY, low to moderate plasticity,	_3.0								Soil Symbol - Graphic representation of subsurface
_	-		(CL) CLAY, high plasticity, (CH)	4.0								material. Material Description -
5	-			_5.0								Account of encountered materials based on ASTM D-2488.
_	_		weathered to unweathered	_6.0 _								Depth - Distance below the
			LIMESTONE, highly to completely weathered	7.0								surface to a strata as measured in the field.
_	-		SHALE, highly to completely weathered	8.0								Sample Type - Method for collecting soil or rock specimens.
_	-											Sample Depth - Collected specimen interval.
10	-		Abbrovictions									Recovery - Percentage of recovered sample material.
-	-		<u>Abbreviations</u> ATD - At the Time of Drilling CFA - Continuous Flight Auger RC - Rock Coring									Standard Penetration Test Blows - Number of blows to drive a splitspoon sampler
-	-		Notes Dashed lines indicate an									three 6" increments with a 140-lb. hammer falling 30".
-			estimated or gradual strata change.									N Value - Number of blows to drive the splitspoon the final foot. These blow counts have
-			Solid lines indicate a more precise, measured depth value.									not been corrected for hammer efficiency or other
15	-											applicable factors. The manual hammer, if used, has an estimated efficiency of
-	-		Splitspoon Sample									60%. The automatic hammer, if used, has an estimated efficiency of 96%.
-	-		Rock Core		\square	16.0 - 17.0						Water Content - The weight of water divided by the
_	-					17.0 - 18.0						weight of oven dried soil, expressed as a percentage.
_	_											Uc - Unconfined compressive strength.
20	_											Comments - Pertinent comments about the conditions encountered.
_	-											Conditions encournered.

Remarks: Additional information about the surface, subsurface or other conditions that could impact the exploration results.

Sheet 1 of 1



BORING RECORD

Project Name Location Client Driller Drill Method Groundwater		iod	Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type See Commen See Commen	Boring No. Project No. Elevation Started Completed Logged By Weather		B-01 61:2606 672 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy						
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, (2 inches) CLAY, silty, orange brown, low to moderate plasticity, firm, moist, (CL), with trace black oxide nodules	0.2		0.0 - 1.5	56	2-2-2	4	22.7		
2.5	670.0					1.5 - 3.0	100	2-3-4	7	34.5		Liquid Limit: 79 Plastic Limit: 24 Plasticity Index: 55
	667.5		CLAY, silty, tan to orange brown with gray mottling, high plasticity, stiff to very stiff, moist to very moist, (CH), with trace to few black oxide nodules	3.5		4.0 - 5.5	94	5-6-8	14	25.3		
_			- with completely to highly weathered rock below approximately 5.2 feet				100	50 (0)	50 (0)			
7.5	665.0		Boring Terminated at Direct Push Refusal	6.8		6.5 - 6.8	100	50/3"	50/3"			
-	662.5	-										
<u>10.0</u>		-										
	660.0		Remarks: (a) Ground surface elevatio	 								ept Plan Sheet 1 of 1

Remarks: (a) Ground surface elevations interpolated to +/- 1-foot based on provided "Concept PlanSheet 1 of 1(Drawing No: 1 – Sheet 1 of 1)", prepared by Sabak, Wilson & Lingo, Inc. dated 9/17/2021.Sheet 1 of 1



BORING RECORD

Project Name Location Client Driller Drill Method Groundwater			Project N	B-02 61:2606 662 (a)							
		Sebec Realty S. Martin Rig Type Geo-Probe 7822DT Direct Push Hammer Type Automatic Not encountered ATD Not					Started Completed Logged By Weather		10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy		
Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
		TOPSOIL, (2 inches) CLAY, tan to orange brown, gray, low to moderate plasticity, slightly moist to moist, (POSSIBLE FILL), with trace organics and black oxide nodules			0.0 - 1.5	100	1-2-3	5			
660.0					1.5 - 3.0	100	3-3-4	7	20.3		
657.5		CLAY, tan brown, high plasticity, very stiff, slightly moist to moist, (CH), with trace organics and black oxide nodules	4.5 _		4.0 - 5.5	100	6-6-7	13	24.2		
655.0		- with completely to highly weathered rock below approximately 6 feet	7.8		6.5 - 7.8	100	9-9-50/3"	50/3"	17.8		
652.5	-	Boring Terminated at Direct Push Refusal									
	-										
		tion trion, tt. Nethod Soil Symbol Soil Symbol	Louisville, K Att Xebec Real r S. Martin Rig Type Method Direct Push Hammer Type Image: Stress of the stress o	Interpretation Louisville, KY r S. Martin Rig Type Getect Method Direct Push Hammer Type Interpretation Getect Image: Stress of the stress of	Louisville, KY Xebec Realty xethod Cec-Prive Method Direct Push Hammer Type Aut Not encountered AID Matterial Description and Classification tile off off tild TOPSOIL_ [2 inches] Output off off off off tild TOPSOIL_ [2 inches] output off off off off tild TOPSOIL_ [2 inches] output off off off off ow to moderate plasticity, sightly moist to moist, (POSSIBLE FILL), with trace organics and black oxide nodules output output output off cs7.s CLAY, tan brown, high plasticity, very stiff, sightly moist to moist, (CH), with trace organics and black oxide nodules output output output end Boring Terminated at Direct Push Top output output output output output end Boring Terminated at Direct Push Refusal output output output output output end Boring Terminated at Direct Push output output output <thoutput< th=""></thoutput<>	Louisville, KY Atteria Xebec Realty Matterial Direct Push Hammer Type Automatic Matterial Description and Classification ti end gradient trace of gradient gradient gradient gradient of gradient gradient of gradient gradient of gradient gradient TOPSOIL (2 inches) gradient Output ti end gradient of gradient of gradient <tholdsymbolicity< th=""> <tholdsymbolicit< td=""><td>Louisville, KY Xebec Realty S. Martin Rig Type Mathematic Ammer Type Mathematic Ammer Type Mathematic Mathematic TopSolL, (2 inches) Question CLAY, tan to anales brown, gray, low to moderate plasticity, slightly moist to moist, (POSSIBLE FILL), with trace organics and black oxide nodules Question CLAY, tan to anales brown, gray, low to moderate plasticity, race organics and black oxide 4.5 4.0 - 5.5 100 CLAY, tan borown, high plasticity, recer organics and black oxide 4.5 4.0 - 5.5 100 CLAY, tan borown, high plasticity, recer organics and black oxide 4.5 4.0 - 5.5 100 CLAY, tan borown, high plasticity, recer organics and black oxide 4.5 4.0 - 5.5 100 Boring Terminated at Direct Push Refusal Refusal 4.5 - 7.8 100 Boring Terminated at Direct Push Refusal Refusal 7.8 4.5 - 7.8 100</td><td>Lucker Station Road Property Project N Ition Louisville, KY Method Direct Push Not encountered AtD Automatic Material Description and Classification $\frac{1}{40}$ $\frac{9}{40}$ $\frac{9}{40}$ Image: Strated CCLAY, tan brown, high plasticity, very stiff, sightly moist to moist, (CH), with trace organics and black oxide 4.5 $4.0 - 5.5$ 100 Image: CLAY, tan brown, high plasticity, very stiff, sightly moist to moist, (CH), with trace organics and black oxide nodules 4.5 $4.0 - 5.5$ 100 $6-6-7$ Strated CLAY, tan brown, high plasticity, very stiff, sightly moist to moist, (CH), with trace organics and black oxide nodules 4.5 $4.0 - 5.5$ 100 $9-9-50/3^\circ$ Strated Refusal Torpeouties of the strategies of the strate</td><td>Louisville, Ky Elevation Stated S. Martin Kebcc Realty Completed Completed Direct Push Hommer Type Geo-Probe 7822DT Completed Completed Moterial Description and Stated Top Stated Material Description and Clossification Top Stated Stated Stated CLAY, tan to orange brown, argu- nodules TopSOIL, [2 inches] Out on coderate plasificity, were static and black oxide Out on coderate plasificity, resc organics and black oxide Automatic Material Description and CLAY, tan to orange brown, argu- nodules Automatic Material Description and CLAY, tan to orange brown, argu- nodules Out on the complete plasificity, very stiff, slightly moist to moist, (PL), with trace organics and black oxide nodules Auto-5.5 100 3-3.4 7 CLAY, tan brown, high plasticity, very stiff, slightly moist to moist, (PL), with trace organics and black oxide nodules Auto-5.5 100 6-6-7 13 Boring Terminated at Direct Push Refusal Top P-9-50/3" 50/3" 50/3" Boring Terminated at Direct Push Refusal Refusal I I I I I I I I I I I I I<td>Torker Station Road Property Project No. Louisville. KY Bevation Stated S. Martin Rig Type Geo-Probe 7822D1 Completed Direct Push Hammer Type Automatic Direct Push Bevation Moterial Description and Classification Top Completed Dog State State TopSoll. (2 inches) Otorange from, grav. Go State State State State TopSoll. (2 inches) Topsoll. (2 inches) Outorange from, grav. Outorange fro</td><td>Internation Tucker Station Road Property Project No. Bievation ition Xebec Realty Started S.Martin Rig Type Geo-Probe 7822DT Description Indextor Material Description and Classification Itig Project No. Elevation Bit watch Itig Material Description and Classification Itig Project No. Elevation Bit watch Itig Operating Itig Project No. Elevation Bit watch Itig Operating Material Description and Classification Itig Project No. Elevation Bit watch Itig Operating Material Description and Classification Itig Project No. Elevation Itig Project No. Elevation Itig Operating Material Description and Classification Itig Project No. Elevation Itig Project No. Elevation Itig Itig Itig Operating Itig Operating Itig Itig</td></td></tholdsymbolicit<></tholdsymbolicity<>	Louisville, KY Xebec Realty S. 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Martin Kebcc Realty Completed Completed Direct Push Hommer Type Geo-Probe 7822DT Completed Completed Moterial Description and Stated Top Stated Material Description and Clossification Top Stated Stated Stated CLAY, tan to orange brown, argu- nodules TopSOIL, [2 inches] Out on coderate plasificity, were static and black oxide Out on coderate plasificity, resc organics and black oxide Automatic Material Description and CLAY, tan to orange brown, argu- nodules Automatic Material Description and CLAY, tan to orange brown, argu- nodules Out on the complete plasificity, very stiff, slightly moist to moist, (PL), with trace organics and black oxide nodules Auto-5.5 100 3-3.4 7 CLAY, tan brown, high plasticity, very stiff, slightly moist to moist, (PL), with trace organics and black oxide nodules Auto-5.5 100 6-6-7 13 Boring Terminated at Direct Push Refusal Top P-9-50/3" 50/3" 50/3" Boring Terminated at Direct Push Refusal Refusal I I I I I I I I I I I I I <td>Torker Station Road Property Project No. Louisville. KY Bevation Stated S. Martin Rig Type Geo-Probe 7822D1 Completed Direct Push Hammer Type Automatic Direct Push Bevation Moterial Description and Classification Top Completed Dog State State TopSoll. (2 inches) Otorange from, grav. Go State State State State TopSoll. (2 inches) Topsoll. (2 inches) Outorange from, grav. Outorange fro</td> <td>Internation Tucker Station Road Property Project No. Bievation ition Xebec Realty Started S.Martin Rig Type Geo-Probe 7822DT Description Indextor Material Description and Classification Itig Project No. Elevation Bit watch Itig Material Description and Classification Itig Project No. Elevation Bit watch Itig Operating Itig Project No. Elevation Bit watch Itig Operating Material Description and Classification Itig Project No. Elevation Bit watch Itig Operating Material Description and Classification Itig Project No. Elevation Itig Project No. Elevation Itig Operating Material Description and Classification Itig Project No. Elevation Itig Project No. Elevation Itig Itig Itig Operating Itig Operating Itig Itig</td>	Torker Station Road Property Project No. Louisville. KY Bevation Stated S. Martin Rig Type Geo-Probe 7822D1 Completed Direct Push Hammer Type Automatic Direct Push Bevation Moterial Description and Classification Top Completed Dog State State TopSoll. (2 inches) Otorange from, grav. Go State State State State TopSoll. (2 inches) Topsoll. (2 inches) Outorange from, grav. Outorange fro	Internation Tucker Station Road Property Project No. Bievation ition Xebec Realty Started S.Martin Rig Type Geo-Probe 7822DT Description Indextor Material Description and Classification Itig Project No. Elevation Bit watch Itig Material Description and Classification Itig Project No. Elevation Bit watch Itig Operating Itig Project No. Elevation Bit watch Itig Operating Material Description and Classification Itig Project No. Elevation Bit watch Itig Operating Material Description and Classification Itig Project No. Elevation Itig Project No. Elevation Itig Operating Material Description and Classification Itig Project No. Elevation Itig Project No. Elevation Itig Itig Itig Operating Itig Operating Itig Itig

Remarks: (a) Ground surface elevations interpolated to +/- 1-foot based on provided "Concept Plan (Drawing No: 1 – Sheet 1 of 1)", prepared by Sabak, Wilson & Lingo, Inc. dated 9/17/2021.



Loco Clier Drille Drill I	atior nt er Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	<u>Y</u> <u> y</u> 	eo-Pr	obe 78221	 DT	Boring Na Project N Elevation Started Complet Logged E Weather	o. ed			B-03 61:2606 652 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, (2 inches) CLAY, silty, tan to orange brown with gray mottling, high plasticity, stiff to hard, slightly moist to moist, (CH), with trace to little black oxide nodules	0.2		0.0 - 1.5	100	2-2-4	6	18.9		
2.5	650.					1.5 - 3.0	100	6-7-9	16	17.5		
5.0	647.					4.0 - 5.5	100	10-10-10	20			
7.5	645.					6.5 - 8.0	100	10-10-12	22	17.0		
 10.0	642.		- with completely to highly weathered rock below approximately 8.5 feet Boring Terminated at Direct Push Refusal	9.7		9.0 - 9.7	100	20-50/2"	50/2"			
	640.		Remarks: (a) Ground surface elevatio									ept Plan Sheet 1 of 1



Loco Clier Drille Drill I	ation nt er Meth		Tucker Station Road Louisville, K Xebec Rea S. Martin Rig Type Direct Push Hammer Type Not encountered	<u>(Y</u> <u>Ity</u> ⊖	eo-Pr	obe 7822 omatic	 	Boring Na Project N Elevation Started Complet Logged I Weather	o. I ed			B-04 61:2606 647 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (6 inches) CLAY, silty, orange brown, moderate plasticity, soft, moist, (CL), with trace black oxide nodules and roots	0.5		0.0 - 1.5	100	1-1-2	3	22.1		
2.5	645.(CLAY, silty, orange brown with gray mottling, highplasticity, stiff to very stiff, moist, (CH), with few to little black oxide nodules	2.0		1.5 - 3.0	100	3-3-5	8	25.3		
5.0	642.					4.0 - 5.5	100	6-6-8	14	22.8		
7.5	640.0		- with completely to highly weathered rock below approximately 6 feet Boring Terminated at Direct Push Refusal	6.8	\times	6.5 - 6.8	100	50/4"	50/4"			
 10.0	637.	5										
	635.0		Remarks: (a) Ground surface elevatic				1.6-					ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill <i>N</i> Grou	ition nt r Meth	iod	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y iy 	eo-Pro	obe 7822[omatic	 DT	Boring No Project No Elevation Started Complete Logged B Weather	o. ed			B-05 61:2606 657 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, with crushed stone, (7 inches) CLAY, silty, tan to orange brown, low to moderate plasticity, very stiff, dry to slightly moist, (CL), with few to little black oxide nodules	0.6		0.0 - 1.5	100	3-4-7	11			
 2.5	<u>655.0</u> 					1.5 - 3.0	83	8-8-9	17	18.7		
5.0	 652.5 		CLAY, silty, tan to yellow brown with gray mottling, high plasticity, hard, slightly moist, (CH), with few black oxide nodules	4.0		4.0 - 5.5	100	10-13-13	26	17.5		
7.5	<u>650.0</u> 					6.5 - 8.0	100	15-15-15	30			
 	 647.5 645.0		- with completely to highly weathered rock below approximately 10.3 feet Boring Terminated at Direct Push Refusal	10.4		9.0 - 10.4	100	13-15-50/5"	50/5"			



Proje Locc Clier Drille Drill <i>N</i> Grou	ation nt r Meth	od	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	<u>Y</u> ty <u>G</u> e	eo-Pr	obe 78221 omatic		Boring No Project N Elevation Started Complete Logged B Weather	o. ed			B-06 61:2606 660 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
			TOPSOIL, (3 inches) CLAY, silty, orange brown, low to moderate plasticity, very stiff, slightly moist, (CL), with trace black oxide nodules and fine roots	<u>0.3</u> 2.0		0.0 - 1.5	100	2-6-7	13			
2.5	<u>657.5</u> 		CLAY, silty, orange brown with gray mottling, high plasticity, very stiff, dry to slightly moist, (CH) with trace black oxide nodules - with completely to highly			1.5 - 3.0	100	3-4-6	10	19.8		
5.0	655.C		Boring Terminated at Direct Push Refusal	5.3		4.0 - 5.3	100	6-16-50/4"	50/4"	14.4		
7.5	652.5											
10.0	650.0											
		-	Remarks: (a) Ground surface elevatio									ept Plan Sheet 1 of 1



Loco Clier Drille Drill	ation nt er Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y ty 	eo-Pr	obe 78221	 	Boring No Project No Elevation Started Complete Logged B Weather	o. ed			B-07 61:2606 670 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (6 inches) CLAY, silty, brown, low to moderate plasticity, stiff, dry to slightly moist, (CL), with trace black oxide nodules and fine roots	0.5		0.0 - 1.5	89	3-4-4	8			
 2.5	<u> </u>		CLAY, silty, orange brown with gray mottling, high plasticity, stiff to hard, dry to slightly moist, (CH), with trace to few black oxide nodules and few rock fragments			1.5 - 3.0	89	6-5-4	9			
5.0	665.0					4.0 - 5.5	100	4-6-7	13			
7.5	662.					6.5 - 8.0	100	7-11-12	23			
 10.0	660.0		- with completely to highly weathered rock below approximately 9.8 feet Boring Terminated at Direct Push Refusal	10.4		9.0 - 10.4	100	17-20-50/5"	50/5"			



Proje Loca Clier Drille Drill N Grou	ition it r Meth	lod	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y hy 	eo-Pr	obe 7822[omatic	 DT	Boring No Project No Elevation Started Complete Logged B Weather	o. ed			B-08 61:2606 672 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
			TOPSOIL, (4 inches) CLAY, silty, orange brown with gray mottling, high plasticity, stiff to hard, dry to moist, (CH), with trace black oxide nodules	0.3		0.0 - 1.5	83	2-2-3	5			
2.5	<u>670.0</u>					1.5 - 3.0	100	6-9-9	18	13.9		
						4.0 - 5.5	100	7-7-7	14	24.0		
5.0	_				$ \begin{tabular}{ c c } \hline \\ \hline $		100			21.0		
7.5						6.5 - 8.0	100	7-9-10	19			
 10.0	 662.5 		- with completely to highly weathered rock below approximately 9.5 feet Boring Terminated at Direct Push Refusal	10.3		9.0 - 10.3	100	12-15-50/3"	50/3"			
	 660.0		Remarks: (a) Ground surface elevatio									ent Plan Sheet 1 of 1



Proie	oct N	amo	Tucker Station Poor	d Bron	ort			Boring No Project No				B-09 61:2606
Loco		ame	Tucker Station Road		berry			Elevation				(00.1-)
Clier								Started				10/22/2021
Drille					robe	7822DT/C	ME-45		ed			11/09/2021
Drill I	Meth		Direct Push/CFA Hammer Type			tomatic		Logged B				B. Emery
Grou	undw	vater	Not encountered	d ATD				Weather				70's Partly Cloudy
						1						
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
				~ <u>0.4</u> ~	\mathbb{N}	0.0 - 1.5	100	2-6-7	13			
			moderate plasticity, very stiff, dry to slightly moist, (CL) with trace roots		$\left \right\rangle$		100	6 7 7	1.4	1/0		
-			CLAY, silty, orange brown, high plasticity, very stiff, dry to moist, (CH), with trace black oxide	2 <u>.5</u>	\vdash	1.5 - 3.0	100	5-7-7	14	16.9		
5	675		nodules			4.0 - 5.5	100	6-8-9	17	27.7		Liquid Limit: 79 Plastic Limit: 26 Plasticity Index: 53
			- with completely to highly weathered rock below approximately 6 feet									Direct Push Refusal at 6.3
 10	670			11.6								Paris Dark Caise at Aver
_			LIMESTONE, moderately weathered, light to medium gray, thin to thick bedded, moderately hard	1 <u>3.0</u>								Begin Rock Coring at Auger Refusal at 11.6 feet.
15	665		LIMESTONE, highly to completely weathered, yellow brown to yellow gray, thin to thick bedded, soft to very soft	1 <u>4.9</u>								
			LIMESTONE, highly to moderately weathered, gray to yellow gray, thin to thick bedded, soft to moderately hard	1 <u>5.9</u> 1 1 <u>6.7</u>		11.6 - 21.6	100	RQD: 87%				
			SHALE, moderately to highly weathered, medium to dark gray, thin to medium bedded, very soft to soft LIMESTONE, slightly weathered to									
	660		unweathered, light to medium gray, medium to massive bedded, moderately hard to hard	21.6								Water recovery projections d
-			Rock coring Terminated									Water recovery maintained throughout core run.
L	I				I	I <u></u>			I	<u> </u>		



Proje Locc Clier Drille Drill / Grou	ation nt er Meth	nod	Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y ty 	eo-Pr	obe 78221	 	Boring No Project No Elevation Started Complete Logged B Weather	o. ed			B-10 61:2606 676 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	675.0		TOPSOIL, (5 inches) CLAY, silty, orange brown to red brown, low to moderate plasticity, stiff, slightly moist, (CL), with trace black oxide nodules	0.4		0.0 - 1.5	100	2-3-4	7	20.5		
2.5			CLAY, silty, orange brown, high plasticity, very stiff to hard, dry to moist, (CH), with trace to few black oxide nodules			1.5 - 3.0	100	7-7-8	15	17.6		
5.0	<u>672.</u>					4.0 - 5.5	100	8-10-10	20			
7.5						6.5 - 8.0	100	8-10-11	21			
 10.0	667.		- with completely to highly weathered rock below approximately 10 feet Boring Terminated at Direct Push Refusal	11.0		9.0 - 10.5		10-10-11	21			



Proje Locc Clier Drille Drill I Grou	ation nt r Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	<u>Υ</u> <u>ty</u> <u>G</u> €	eo-Pr	obe 78221		Boring No Project No Elevation Started Complete Logged E Weather	o. ed			B-11 61:2606 666 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (3 inches) CLAY, silty, brown, low to moderate plasticity, firm, moist, (CL)	0.3		0.0 - 1.5	100	1-2-2	4	24.1		Liquid Limit: 81 Plastic Limit: 28
2.5	662.5		CLAY, silty, orange brown with	3.5		1.5 - 3.0	78	3-3-5	8	30.8		Plasticity Index: 53
5.0			CLAY, silty, orange brown with gray mottling, high plasticity, stiff, moist to very moist, (CH), with trace black oxide nodules - with completely to highly weathered rock below approximately 4.5 feet Boring Terminated at Direct Push	5.4		4.0 - 5.4	100	5-9-50/5"	50/5"			
-	<u>660.0</u> 	-	Refusal									
7.5	657.5											
10.0												
	655.0		Remarks: (a) Ground surface elevatic								<u></u>	ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill <i>N</i> Grou	ition it r Meth	nod	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y ty 	eo-Pr	obe 78221	T	Boring No Project N Elevation Started Complet Logged E Weather	o. ed			B-12 61:2606 663 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_	<u>662.</u>		TOPSOIL, (3 inches) CLAY, silty, orange brown, low plasticity, soft, moist, (CL), with trace fine roots	0.3		0.0 - 1.5	100	1-2-1	3			
2.5			CLAY, silty, orange brown, high plasticity, very stiff to hard, dry to moist, (CH), with trace black oxide nodules			1.5 - 3.0	100	5-6-7	13	19.3		
5.0						4.0 - 5.5	78	10-10-11	21	21.1		
 7.5	 		- light gray below approximately 7.2 feet			6.5 - 8.0	100	9-10-14	24	26.0		
 10.0			- with completely to highly weathered rock below approximately 9 feet Boring Terminated at Direct Push Refusal	9.3	\ge	9.0 - 9.3	100	50/4"	50/4"			
	<u>652.</u>	_	Remarks: (a) Ground surface elevatio									ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill <i>N</i> Grou	ition nt r Meth	od	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y ty 	eo-Pro	obe 78221 omatic		Boring No Project N Elevation Started Complete Logged E Weather	o. I			B-13 61:2606 659 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (3 inches) GRAVEL, crushed stone, clayey, (FILL) CLAY, silty, brown, low to moderate plasticity, stiff, slightly moist to moist, (CL), with trace black oxide nodules and organics	0.3 0.5		0.0 - 1.5	100	3-3-3	6	22.6		
 2.5			CLAY, silty, tan brown with gray mottling, high plasticity, very stiff to hard, slightly moist to moist, (CH), with few black oxide nodules			1.5 - 3.0	100	5-8-8	16	24.8		
5.0	 		- with completely to highly weathered rock below approximately 4 feet			4.0 - 5.5	100	14-21-17	38			
7.5			Boring Terminated at Direct Push Refusal	6.8	\times	6.5 - 6.8	100	50/4"	50/4"			
<u> </u>		-	Remarks: (a) Ground surface elevatio									ept Plan Sheet 1 of 1



Loco Clier Drille Drill	ation nt er Meth		Tucker Station Road Louisville, K Xebec Realt S. Martin/D. UnderwoodRig Type C Direct Push/CFA Hammer Type Not encountered Not encountered	Y i y Geo <u>-Pr</u>	robe			Boring No Project N Elevation Started 5 Complet Logged E Weather	o. ed			B-14 61:2606 677 (a) 10/22/2021 11/09/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-	675		TOPSOIL, (2 inches) // CLAY, silty, orange brown, moderate plasticity, soft, moist, (CL), with few black oxide nodules CLAY, silty, orange brown, high plasticity, very stiff, moist to very moist, (CH), with few black oxide nodules	2.0_		0.0 - 1.5	100	1-2-1 3-4-6	3 10	22.3 31.4		
5	670		- with completely to highly weathered rock below approximately 5 feet		X	4.0 - 5.5 6.5 - 6.8	56 100	7-5-8 50/3"	13 50/3"	34.5		Direct Push Refusal at 6.8
<u> </u>	665		LIMESTONE, slightly weathered to unweathered, light to medium gray, thin to thick bedded, moderately hard,	9.0								Begin Rock Coring at Auger Refusal at 9 feet.
<u>15</u> 	660		- with interbedded shale below approximately 18.5 feet	19.0		9.0 - 19.0	98	RQD: 90%				
20	655	_	Remarks: (a) Ground surface elevation	19.0								water recovery maintained throughout core run. ept Plan Sheet 1 of 1



Project Name Location Client Driller Drill Method Groundwater	Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y	eo-Pr	obe 78221	 	Boring No Project No Elevation Started Complete Logged B Weather	o. ed			B-15 61:2606 678 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft. Elevation, ft. Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	TOPSOIL, (3 inches) CLAY, silty, brown, low to moderate plasticity, soft, moist, (CL)	0.3		0.0 - 1.5	100	1-1-1 4-5-6	2	23.8 29.8		Liquid Limit: 69 Plastic Limit: 26 Plasticity Index: 43
	CLAY, silty, orange brown, high plasticity, very stiff, moist, (CH), with trace black oxide nodules Boring Terminated at Direct Push Refusal	3.5								



Proje Loca Clier Drille Drill N Grou	ition it r Meth	od	Tucker Station Roc Louisville, Xebec Rec S. Martin Rig Type Direct Push Hammer Type Not encountered	KY alty Ge	eo-Pr	obe 78221 omatic	 	Boring No Project N Elevation Started Complete Logged E Weather	o. ed	B-16 61:2606 668 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy		61:2606 668 (a) 10/22/2021 10/22/2021 B. Emery
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	<u>667.5</u> 		TOPSOIL, (4 inches) CLAY, silty, brown, moderate plasticity, firm, moist, (CL)	0.3 _		0.0 - 1.5	100	2-2-2	4	23.8		
2.5	 665.0		- with completely to highly weathered rock below approximately 2.3 feet Boring Terminated at Direct Push Refusal	2.8		1.5 - 3.0	89	5-15-50/4"	50/4"			
		-										
5.0	 											
7.5	 660.0											
		-										
10.0	 657.5											
		-										



Proje Locc Clier Drille Drill <i>N</i> Grou	ition nt r ∧eth	od	Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y Iy 	eo-Pr	obe 78221 omatic	 	Boring No Project N Elevation Started Complet Logged E Weather	o. ed	B-17 61:2606 663 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy		61:2606 663 (a) 10/21/2021 10/21/2021 B. Emery
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	<u>662.5</u> 		CLAY, silty, orange brown, CLAY, silty, orange brown, moderate plasticity, dry, (POSSIBLE FILL), with trace rock fragments	0.2		0.0 - 1.5	83	6-5-5	10			
2.5	 660.0		CLAY, silty, red brown, moderate plasticity, very stiff to hard, dry to slightly moist, (CL)	2.0		1.5 - 3.0	100	5-8-13	21	21.4		
5.0	_		- with completely to highly weathered rock below approximately 3.7 feet Boring Terminated at Direct Push	4.7		4.0 - 5.5	100	20-50/3"	50/3"	12.4		
	<u>657.5</u> 		Refusal									
7.5	 655.0											
10.0	 652.5											
		-	Remarks: (a) Ground surface elevation									ent Plan Sheet 1 of 1



Loco Clier Drille Drill I	ation nt er Meth		Tucker Station Rog Louisville, Xebec Reg S. Martin Rig Type Direct Push Hammer Type Not encountered	KY alty Ge	eo-Pr	obe 78221 omatic	 	Boring Na Project N Elevation Started Complet Logged B Weather	o. I ed		B-18 61:2606 673 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy	
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_	672.5		TOPSOIL, (18 inches)	1.5_		0.0 - 1.5	94	4-3-1	4			
2.5	670.0		plasticity, stiff, slightly moist to moist (CL)			1.5 - 3.0	56	3-4-5	9	21.8		
	667.		CLAY, silty, orange brown, high plasticity, very stiff, moist, (CH), with few black oxide nodules - with completely to highly weathered rock below approximately 5 feet Boring Terminated at Direct Push Refusal	<u>4.2</u> 5.3		4.0 - 5.5	78	5-7-50/4"	50/4"			
 7.5 	665.0	- - - -										
 10.0	662.5											



Proje Locc Clier Drille Drill M Grou	ition nt r ∧eth	od	Tucker Station Roac Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y	eo-Pr	obe 78221	 	Boring No Project N Elevation Started Complet Logged E Weather	o. ed			B-19 61:2606 675 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
			TOPSOIL, (21 inches)			0.0 - 1.5	100	1-1-1	2			
2.5	672.5		CLAY, silty, orange brown, moderate plasticity, firm, moist, (CL) with trace black oxide nodules	1.8		1.5 - 3.0	94	2-2-2	4	25.9		
			CLAY, silty, orange brown, high plasticity, stiff, moist, (CH), with little black oxide nodules	3.5								
5.0	<u>670.0</u>				Å	4.0 - 5.5	100	3-4-5	9			
7.5	 667.5		- with completely to highly weathered rock below approximately 7 feet Boring Terminated at Direct Push	7.3	X	6.5 - 7.3	100	6-50/4	50/4			
-		-	Refusal									
 10.0	665.0)										
		-	Remarks: (a) Ground surface elevatio									ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill M Grou	ition nt r Meth	nod	Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y iy 	eo-Pr	obe 78221 omatic		Boring No Project No Elevation Started Complete Logged E Weather	o. ed	6 6 10/2 10/2 10/2 B. 70's Pa		B-20 61:2606 680 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, (6 inches) CLAY, silty, orange brown, low to moderate plasticity, stiff, moist, (CL), with trace black oxide nodules and fine roots	<u>0.5</u>		0.0 - 1.5	100	2-2-3	5	22.2		
2.5			CLAY, silty, orange brown, high plasticity, very stiff, slightly moist to moist, (CH), with few black oxide nodules			1.5 - 3.0	89	5-5-6	11	25.3		Liquid Limit: 88 Plastic Limit: 38 Plasticity Index: 50
5.0			- with completely to highly weathered rock below approximately 4 feet Boring Terminated at Direct Push Refusal	4.7		4.0 - 4.7	100	15-50/4	50/4			
	_	-										
7.5	<u>672.</u>	-										
10.0	 670.0	-										
			Remarks: (a) Ground surface elevatior								<u></u>	ept Plan Sheet 1 of 1



Loco	Project Name Location Client Driller Drill Method	Tucker Station Road Louisville, K Xebec Real	Ϋ́	perty	,		Boring No Project N Elevation Started	о.			B-21 61:2606 670 (a) 10/22/2021	
Drille Drill I	er Met	hod water	S. Martin Rig Type Direct Push Hammer Type See comment	<u> </u>		obe 78221 tomatic		Complete Logged E Weather				10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, (6 inches) CLAY, silty, orange brown, high plasticity, stiff, moist to very moist, (CH), with few black oxide nodules	0.5		0.0 - 1.5	94	2-3-4	7	31.4		
2.5	667					1.5 - 3.0	100	5-5-4	9	21.4		
-			- with completely to highly weathered rock below approximately 3.8 feet	4.7		4.0 - 4.7	100	19-50/2"	50/2"			Groundwater seepage observed at rock/soil interface.
5.0	665	.0	Boring Terminated at Direct Push Refusal									
7.5	662	.5										
		_										
<u> </u>	660	.0										
		_	Remarks: (a) Ground surface elevation									ept Plan Sheet 1 of 1



Project Name Location Client Driller Drill Method Groundwate	Louisville, K Xebec Real S. Martin Rig Type Direct Push	<u>Y</u> ty <u>G</u> e	eo-Pr	obe 78221 omatic	 	Boring No Project N Elevation Started Complet Logged E Weather	o. 1 ed 3y		B-22 61:2606 678 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy	
Scale, ft. Elevation, ft. Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
<u></u>	TOPSOIL, (4 inches) CLAY, silty, orange brown, high plasticity, stiff, moist, (CH), with few black oxide nodules	0.3		0.0 - 1.5	100	1-2-3	5	23.9		
	- with completely to highly weathered rock below approximately 2 feet	2.3	\square	1.5 - 2.3	100	5-50/3"	50/3"			
2.5	Boring Terminated at Direct Push Refusal									



Loco Clier Drille Drill	ation nt r Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y hy 	eo-Pr	obe 7822 tomatic		Boring No Project N Elevation Started Complete Logged E Weather	o. ed			61:2606 679 (a) 10/22/2021 10/22/2021
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-	677.		TOPSOIL, (7 inches) CLAY, silty, orange brown, low plasticity, soft, moist, (CL), with trace black oxide nodules and fine roots	0.6		0.0 - 1.5	100	1-1-2	3	25.1		Liquid Limit: 43 Plastic Limit: 24 Plasticity Index: 19
 			CLAY, silty, orange brown, high plasticity, very stiff, moist, (CH), with few black oxide nodules	2.0		1.5 - 3.0	100	2-4-7	11	27.8		
5.0	675.(- with completely to highly weathered rock below approximately 4.8 feet Boring Terminated at Direct Push Refusal	5.0		4.0 - 5.0	83	7-7-50/0"	50/0"			
	672.	5										
 10.0	<u>670.(</u> 	-										



Loco Clier Drille Drill I	ation nt r Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y hy 	eo-Pr	obe 7822 omatic		Boring No Project No Elevation Started Complete Logged E Weather	o. ed	B-24 61:2606 670 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy		61:2606 670 (a) 10/22/2021 10/22/2021 B. Emery
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-	·		TOPSOIL, (3 inches) CLAY, silty, tan brown, low plasticity, stiff, moist to very moist, (CL), with few black oxide nodules and trace fine roots	0.3		0.0 - 1.5	100	2-2-3	5	28.5		
 	 667. <u>:</u>	5	- with completely to highly weathered rock below approximately 2.4 feet Boring Terminated at Direct Push Refusal	2.9		1.5 - 2.9	100	9-13-50/5"	50/5"			
5.0	665.0											
		_										
7.5	662.	5										
10.0	660.0	2										
		_	Remarks: (a) Ground surface elevation									ent Plan Sheet 1 of 1



Loco Clier Drille Drill I	atioi ht er Met		Tucker Station Road Louisville, K Xebec Rea S. Martin Rig Type Direct Push Hammer Type Not encountered	(Y Ity <u>G</u> e	eo-Pro	obe 78221		Boring No Project N Elevation Started Complete Logged E Weather	o. 1 ed 3y	61:2606 672 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy		672 (a) 10/21/2021 10/21/2021
Scale, ft.	Elevation, ft.	0,	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
 	665		TOPSOIL, (4 inches) CLAY, silty, brown gray, low to 1 moderate plasticity, soft, moist, 1 (POSSIBLE FILL) CLAY, silty, orange brown, high plasticity, very stiff, moist, (CH), with few to little black oxide nodules - with completely to highly weathered rock below approximately 2 feet Boring Terminated at Direct Push Refusal	0.3 0.6 1 2.8		0.0 - 1.5	100	2-2-3 7-4-50/3"	5	22.5		
 	 662 											



Proje Locc Clier Drille Drill I Grou	ation nt r Meth	od	Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y <u>G</u> e	eo-Pr	obe 7822 omatic		Boring Na Project N Elevation Started Complete Logged E Weather	o. ed By		B-26 61:2606 682 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy	
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (6 inches) CLAY, silty, tan brown, low plasticity, stiff, slightly moist, (CL), with trace black oxide nodules	0.5		0.0 - 1.5	100	3-3-4	7			
2.5	680.0		CLAY, silty, orange brown with gray mottling, high plasticity, very stiff, moist, (CH), with little black oxide nodules	_1.7 _		1.5 - 3.0	100	5-6-6	12	20.4		
5.0	 677.5		- with completely to highly weathered rock below approximately 5.2 feet Boring Terminated at Direct Push	5.4		4.0 - 5.3	100	6-6-50/4"	50/4"	26.1		
7.5	675.0	-	Refusal									
	672.5	-										
<u>10.0</u>		-										



Proje Locc Clier Drille Drill I Grou	ition it r Meth	nod	Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y iy 	eo-Pr	obe 78221 omatic	 	Boring Na Project N Elevation Started Complet Logged E Weather	o. ed			B-27 61:2606 669 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	667.5		TOPSOIL, (3 inches) CLAY, silty, orange brown, low plasticity, stiff to very stiff, slightly moist to moist, (CL), with trace fine roots and black oxide nodules	0.3		0.0 - 1.5	94	3-3-4	7			
<u>2.5</u>						1.5 - 3.0	100	7-6-5	11	22.1		
5.0	<u>665.(</u> 			5.8		4.0 - 5.5	100	5-6-6	12	25.0		
 			CLAY, silty, orange brown with light brown mottling, high plasticity, very stiff, slightly moist, (CH), with trace black oxide nodules			6.5 - 8.0	100	8-9-9	18			
 10.0			- with completely to highly weathered rock below approximately 9.5 feet Boring Terminated at Direct Push Refusal	9.9		9.0 - 9.9	100	16-50/5"	50/5"			
	657.5		Remarks: (a) Ground surface elevatior									ept Plan Sheet 1 of 1



Locc Clier Drille Drill N	nt	od	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	(Y ty 	eo-Pr	obe 78221 omatic	 	Boring No Project N Elevation Started Complet Logged B Weather	o. I			B-28 61:2606 659 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.		Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	657.5		TOPSOIL, (5 inches) CLAY, silty, brown with light gray mottling, low to moderate plasticity, stiff to very stiff, slightly moist, (CL), with trace fine roots and trace to little black oxide nodules	0.4		0.0 - 1.5	100	2-2-2	4	23.3		
2.5 — — — 5.0	655.0					1.5 - 3.0 4.0 - 5.5	100	3-3-3 5-5-6	6	22.7		
 	<u>652.5</u>		CLAY, silty, tan to orange brown, high plasticity, very stiff to hard, slightly moist, (CH), with few to little black oxide nodules	6.0		6.5 - 8.0	100	8-9-12	21			
 10.0	<u>650.0</u> 		- with completely to highly weathered rock below approximately 9.5 feet Boring Terminated at Direct Push Refusal	9.8		9.0 - 9.8	100	23-50/3"	50/3"			



Loco Clier Drille Drill I	ntion nt r Meth		Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y <u>G</u> e	eo-Pr	obe 7822[omatic	 DT	Boring Na Project Na Elevation Started Complete Logged B Weather	o. ed			B-29 61:2606 667 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (4 inches) CLAY, silty, brown, low to moderate plasticity, stiff, slightly moist to very moist, (CL), with few to little black oxide nodules and trace fine roots	_0.3 _		0.0 - 1.5	100	2-2-3	5	21.3		
 	<u>665.0</u> 					1.5 - 3.0	100	3-4-4	8	30.0		
5.0	 662.5 		CLAY, silty, tan to orange brown with light gray mottling, high plasticity, very stiff to hard, slightly moist to moist, (CH), few to little black oxide nodules	3.5		4.0 - 5.5	100	4-6-8	14			
 7.5	 660.0 					6.5 - 8.0	100	10-11-11	22			
<u> </u>			- with completely to highly weathered rock below approximately 9.5 feet Boring Terminated at Direct Push Refusal	10.3		9.0 - 10.3	100	17-17-50/4"	50/4"			



Loco Clier Drille Drill I	nt	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	<u>Y</u> <u> y</u> 	eo-Pro	obe 78221 omatic		Boring No Project No Elevation Started Complete Logged B Weather	o. ed			B-30 61:2606 674 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	672.5	TOPSOIL, (4 inches) CLAY, silty, orange brown, low plasticity, stiff, moist, (CL), with trace black oxide nodules and fine roots	<u>0.3</u> 2.0		0.0 - 1.5	100	3-3-2	5	21.4		Liquid Limit: 36 Plastic Limit: 21 Plasticity Index: 15
<u>2.5</u>		CLAY, silty, orange brown with dark brown mottling, high plasticity, very stiff, moist to very moist, (CH), with few black oxide nodules			1.5 - 3.0	100	5-5-6	11	31.5		
5.0	6667.5	weathered rock below approximately 4 feet Boring Terminated at Direct Push Refusal	<u>5.1</u>		4.0 - 5.2	100	13-18-50/2"	50/2"			
 	665.0										
<u> </u>	662.5										



Loco Clier Drille Drill I	ation nt r Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	<u>Y</u> ty <u>G</u> e	eo-Pr	obe 78221	 	Boring No Project N Elevation Started Complete Logged E Weather	o. ed			B-31 61:2606 680 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
5.0			TOPSOIL, (8 inches) CLAY, silty, brown, moderate plasticity, stiff to very stiff, moist to very moist, (CL), with little black oxide nodules - with completely to highly weathered rock below approximately 2.2 feet Boring Terminated at Direct Push Refusal	2.9		0.0 - 1.5	22 100 82	2-2-3 8-10-50/5"	5	29.3		
		_	Remarks: (a) Ground surface elevatio									ent Plan Sheet 1 of 1



Loco Clier Drille Drill	ation nt er Meth		Tucker Station Road Louisville, K Xebec Rea S. Martin/D. UnderwoodRig Type Direct Push/CFA Hammer Type Not encountered	(Y ty Geo <u>-Pi</u>	robe			Boring No Project No Elevation Started 5 Complete Logged B Weather	o. ed			B-32 61:2606 684 (a) 10/21/2021 11/08/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (4 inches) CLAY, silty, brown, moderate plasticity, firm to very stiff, moist, (CL), with little black oxide nodules and fine roots	<u>, ∧ 0.3</u> ∠		0.0 - 1.5	100 100	2-2-2 4-6-6	4 12	23.9		
	680		CLAY, silty, orange brown with gray and light brown mottling, high plasticity, very stiff, moist, (CH) - with weathered rock below approximately 5.5	4.0		4.0 - 5.5	100	6-8-8	16	27.4		Liquid Limit: 63 Plastic Limit: 30 Plasticity Index: 33 Direct Push Refusal at 5.7
 10 	675		LIMESTONE, slightly weathered to unweathered, light to medium gray, thin to thick bedded, moderately hard	9.0								Begin Rock Coring at Auger Refusal at 9 feet.
 	670					9.0 - 19.0	95	RQD: 93%				
20	<u>665</u>	-	Rock coring Terminated	19.0								Water recovery maintained throughout core run. ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill I Grou	ation nt r Meth	od	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y ty 	eo-Pr	obe 7822 tomatic		Boring Na Project N Elevation Started Complet Logged E Weather	o. ed			B-33 61:2606 682 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, (3 inches) CLAY, silty, brown, low to moderate plasticity, firm, moist, (CL), with trace black oxide nodules	0.3		0.0 - 1.5	100	1-2-2	4	24.8		
2.5	<u>680.(</u> 		CLAY, silty, tan to orange brown with gray mottling, high plasticity, stiff to very stiff, moist to very moist, (CH), with few to little black oxide nodules	2.0		1.5 - 3.0	100	5-5-6	11	29.8		
5.0	<u>677.5</u>					4.0 - 5.5	100	4-4-5	9	36.4		
7.5	 675.0		- with completely to highly weathered rock below approximately 6 feet Boring Terminated at Direct Push Refusal	7.0	X	6.5 - 7.0	100	15-50/0"	50/0"			
10.0	 672.5	-										
	670.0		Remarks: (a) Ground surface elevatio									ept Plan Sheet 1 of 1



Locc Clier Drille Drill N	ition it r Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y hy 	eo-Pr	obe 78221 omatic		Boring No Project No Elevation Started Complete Logged E Weather	o. ed			B-34 61:2606 672 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	_		TOPSOIL, (2 inches) CLAY, silty, light brown, high plasticity, stiff, moist, (CH), with trace to few black oxide nodules	0.2		0.0 - 1.5	94	2-2-4	6	23.9		
2.5	<u>670.</u>		- with completely to highly weathered rock below approximately 2.2 feet Boring Terminated at Direct Push	2.7		1.5 - 2.8	88	5-12-50/2"	50/2"			
	_	_	Refusal									
5.0	<u>667.</u> 	5										
		-										
7.5	_											
		5										
10.0	_	-										
	660.0		Remarks: (a) Ground surface elevatio									ent Plan Sheet 1 of 1



		lame	Tucker Station Road		perty			Boring No Project N	о.			B-35 61:2606
Loco Clier		1	Louisville, K Xebec Rea					Elevation Started	l			662 (a) 10/21/2021
Drille			S. Martin Rig Type		eo-Pr	obe 7822I	DT	Complet	ed			10/21/2021
Drill I			Direct Push Hammer Type	-	Aut	omatic		Logged I	Зу			B. Hasanzadeh
Grou	Indv	vater	Not encountered	d ATD				Weather				50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (4 inches) CLAY, silty, brown, low to moderate plasticity, moist, (FILL), with few to little crushed stone	0.3		0.0 - 1.5	89	2-2-6	8	13.7		
2.5	<u>660.(</u> 		CLAY, silty, brown, moderate plasticity, very stiff, moist to very moist, (CL), with few to little black oxide nodules	1.8		1.5 - 3.0	83	4-5-6	11	28.5		
5.0	657.		CLAY, silty, tan to orange brown with gray mottling, high plasticity, very stiff, slightly moist to moist, (CH), with few to little black oxide nodules	3.5		4.0 - 5.5	100	5-5-6	11			
	655.0		- with completely to highly weathered rock below approximately 7 feet Boring Terminated at Direct Push Refusal	7.2		6.5 - 7.2	100	8-50/2"	50/2"			
 	<u>652.</u> 	_										



Proje Locc Clier Drille Drill I Grou	ation nt er Meth	iod	Tucker Station Road Louisville, K' Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y iy <u>G</u> e	eo-Pr	obe 7822[omatic	 	Boring No Project N Elevation Started Complet Logged E Weather	o. ed			B-36 61:2606 678 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	677.5		TOPSOIL, (2 inches) CLAY, silty, brown, low to moderate plasticity, dry, (FILL), with little crushed stone and asphalt fragments, and trace organics CLAY, silty, tan to orange brown, high plasticity, stiff to very stiff, moist, (CH), with trace black oxide nodules			0.0 - 0.8	100 89	3-50/3" 2-4-5	50/3" 9	16.9		
	675.0		- with completely to highly weathered rock below approximately 4.4 feet Boring Terminated at Direct Push	4.9		4.0 - 4.9	100	14-50/5"	50/5"			
	672.5	-	Refusal									
 10.0	<u>670.0</u> 	-										
		-	Remarks: (a) Ground surface elevation									ept Plan Sheet 1 of 1



Loco Clier Drille Drill	ation nt		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y	eo-Pr	obe 78221 omatic	 	Boring No Project N Elevation Started Complet Logged B Weather	o. ed			B-37 61:2606 668 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-	667.5		GRAVEL, crushed stone, clayey, (8 inches) CLAY, silty, brown, gray brown, gray, low to moderate plasticity, dry to very moist, (FILL), with few to some crushed stone and few organics	0.7		0.0 - 1.5	94	9-4-4	8			
2.5 — — 5.0	<u>665.0</u> 662.5					1.5 - 3.0 4.0 - 5.5	72	3-4-3 2-2-2	7	23.4 34.8		
	660.0		Boring Terminated at Direct Push	8.5		6.5 - 8.0	22	10-2-2	4			
 10.0 	657.5		Refusal Remarks: (a) Ground surface elevatio									ept Plan Sheet 1 of 1



Loco Clier Drille Drill I	ition nt r Meth		Tucker Station Road Louisville, K Xebec Rea S. Martin Rig Type Direct Push Hammer Type Not encountered	(Y ty 	eo-Pr	obe 7822 omatic		Boring No Project No Elevation Started Complete Logged E Weather	o. ed			B-38 61:2606 678 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
2.5	<u>677.</u>		TOPSOIL, (6 inches) CLAY, silty, brown, low to moderate plasticity, stiff, moist, (CL), with trace black oxide nodules CLAY, silty, tan to orange brown, high plasticity, stiff to very stiff, moist, (CH), with trace black oxide nodules - with completely to highly weathered rock below approximately 2.5 feet Boring Terminated at Direct Push Refusal	0.5	2G	0.0 - 1.5 1.5 - 2.9	± 83 100	2-2-3 5-11-50/5"	5 50/5"	WC		



Loco Clier Drille Drill <i>I</i>	ation nt er Meth		Tucker Station Road Louisville, K Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y iy 	eo-Pr	obe 78221 omatic	 	Boring No Project No Elevation Started Complete Logged E Weather	o. ed			B-39 61:2606 676 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	675.0		TOPSOIL, (1-inch) / CLAY, silty, red brown, low to moderate plasticity, moist, (FILL), with few crushed stone - - mostly crushed asphalt below approximately 0.5 feet CLAY, silty, brown, moderate plasticity, stiff, moist, (CL), with few black oxide nodules -	<u>_1.5</u> _		0.0 - 1.5 1.5 - 3.0	72	18-5-2 3-4-5	7 9	22.0		
5.0	672.5					4.0 - 5.5	100	3-4-5	9	23.1		
	<u>670.(</u> 		CLAY, silty, brown to tan brown, high plasticity, stiff, slightly moist to moist, (CH), with few black oxide nodules - with completely to highly weathered rock below approximately 7.1 feet Boring Terminated at Direct Push Refusal	6.0		6.5 - 7.6	100	4-14-50/1"	50/1"			
 10.0	665.0	-										



								Boring No	Э.			B-40
		lame	Tucker Station Road		perty	,		Project N				61:2606
Locc Clier			Louisville, K Zebec Real					Elevation Started				<u> </u>
Drille			<u>S. Martin</u> Rig Type		eo-Pr	obe 7822[DT	Complete	ed			10/21/2021
Drill I	Meth	nod	Direct Push Hammer Type			omatic		Logged E		-		B. Hasanzadeh
Grou	undv	vater	Not encountered	ATD				Weather				50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	c, tsf	Comments
	Ē	S S S			S	ы С С С С С	Å	Ste Pe Te	Z	≥ŭ	Uc,	
	677.	· · · ·	TOPSOIL, (5 inches) CLAY, silty, brown, low to moderate plasticity, stiff, moist, (CL), with few black oxide nodules	0.4		0.0 - 1.5	94	3-2-3	5	22.6		
2.5	675.0					1.5 - 3.0	100	3-3-3	6	24.8		
5.0			CLAY, silty, brown to orange brown, high plasticity, stiff, slightly moist to very moist, (CH), with few to little black oxide nodules	3.5		4.0 - 5.5	94	3-4-4	8	27.0		Liquid Limit: 75 Plastic Limit: 34 Plasticity Index: 41
	672.		- with completely to highly weathered rock below approximately 7.1 feet	7.8		6.5 - 7.8	100	6-6-50/3"	50/3"			
10.0	<u>670.(</u> 667.(<u>-</u> -	Boring Terminated at Direct Push Refusal									



Loco Clier Drille Drill I	ation nt er Meth		Tucker Station Road Louisville, K Xebec Rea S. Martin/D. UnderwoodRig Type Direct Push/CFAHammer Type Not encountered	Y ty Geo <u>-P</u>	robe			Boring No Project N Elevation Started Complete Logged E Weather	o. ed			B-41 61:2606 683 (a) 10/21/2021 11/08/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	680		TOPSOIL, (3 inches) CLAY, silty, brown to tan brown, low to moderate plasticity, stiff, slightly moist, (CL), with few black oxide nodules CLAY, silty, brown to tan brown with orange and gray mottling, high plasticity, very stiff, slightly moist to moist, (CH), with few to little black oxide nodules	<u>0.3</u> 1.5		0.0 - 1.5 1.5 - 3.0 4.0 - 4.8	100 100 100	1-2-3 8-9-8 7-50/3"	5 17 50/3"	23.2 23.0		
	675 		 with completely to highly weathered rock below approximately 4.5 feet LIMESTONE, slightly weathered to unweathered, light to medium gray, thin to massive bedded, moderately hard 	7.0		7.0 - 22.0	94	RQD: 89%				Direct Push Refusal at 4.8 Begin Rock Coring at Auger Refusal at 7 feet.
	660		Rock coring Terminated Remarks: (a) Ground surface elevatic	22.0								Water recovery maintained throughout core run. ept Plan Sheet 1 of 1



Locc Clier Drille Drill N	nt	Tucker Station Roac Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y ty 	eo-Pro	obe 78221 omatic		Boring No Project N Elevation Started Complet Logged E Weather	o. ed By			B-42 61:2606 658 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft. Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	<u>657.5</u> / <u>1</u> .34/	TOPSOIL, (6 inches) CLAY, silty, medium to dark brown, moderate plasticity, stiff, moist, (CL), with trace fine roots CLAY, silty, orange brown, high plasticity, stiff to very stiff, moist, (CH), with trace black oxide	0.5		0.0 - 1.5	100	2-2-3	5			
2.5		nodules		X	1.5 - 3.0	83	3-3-5	8	26.3		
5.0	 	- with completely to highly weathered rock below approximately 5.2 feet Boring Terminated	5.5		4.0 - 5.5	100	6-8-8	16			
7.5	 650.0										
10.0											
	<u>647.5</u> 										



Proje Locc Clier Drille Drill <i>I</i> Grou	ation nt er Meth	iod	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	Y ty 	eo-Pro	obe 78221 omatic	 DT	Boring No Project N Elevation Started Complet Logged B Weather	o. 1 ed 3y			B-43 61:2606 648 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_	647.5		TOPSOIL, (4 inches) CLAY, silty, orange brown, high plasticity, stiff to very stiff, dry to moist, (CH), with trace to few black oxide nodules	0.3		0.0 - 1.5	100	2-2-4	6	21.8		
2.5	645.0		- with light gray mottling below approximately 1.7 feet			1.5 - 3.0	100	3-4-4	8			
5.0	642.5			5.5		4.0 - 5.5	100	5-7-7	14			
 7.5			Boring Terminated	3.3								
	640.0	-										
<u>10.0</u>	637.5	5										



Proje Loca Clier Drille Drill <i>N</i> Grou	tion it r Netho	bd	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	(Y ty 	eo-Pr	obe 78221 omatic	 	Boring No Project N Elevation Started Complete Logged E Weather	o. ed			B-44 61:2606 646 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	<u></u> 645.0		TOPSOIL, (5 inches) CLAY, silty, orange to tan brown, moderate plasticity, stiff to very stiff, dry to slightly moist, (CL), with trace black oxide nodules	0.4		0.0 - 1.5	100	2-2-3	5	11.7		
 	 					1.5 - 3.0	100	2-2-3	5	21.6		
5.0	 640.0		- with completely to highly			4.0 - 5.5	78	5-7-6	13			
7.5			weathered rock below approximately 6.1 feet Boring Terminated at Direct Push Refusal	6.8		6.5 - 6.8	100	50/4"	50/4"			
 10.0	<u>637.5</u> 											
	<u>635.0</u>		2emarks: (a) Ground surface elevatic								_	ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill <i>I</i> Grou	ation nt r Meth	od	Tucker Station Road Louisville, KY Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	y	eo-Pr	obe 78221 omatic		Boring No Project N Elevation Started Complete Logged E Weather	o. ed By			B-45 61:2606 678 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	477 5		GRAVEL, crushed stone, clayey, (FILL) CLAY, silty, orange brown, moderate plasticity, stiff to very stiff, slightly moist, (CL), with few	_1.0_		0.0 - 1.5	72	10-9-3	12			
2.5	 675.0		CLAY, silty, orange brown, high plasticity, very stiff, moist, (CH), with few black oxide nodules	_2.0 _		1.5 - 3.0	100	4-5-5	10	21.8		
5.0						4.0 - 5.5	44	6-6-7	13			
	672.5		Boring Terminated	5.5								
7.5	670.0	-										
10.0	 667.5											
			Remarks: (a) Ground surface elevation									ent Plan Sheet 1 of 1



Loco Clier Drille Drill I	nt	Louisville, I Xebec Rea S. Martin Rig Type Direct Push Hammer Type	(Y Ity <u>G</u> e	eo-Pr	obe 78221 tomatic		Boring Na Project N Elevation Started Complet Logged F Weather	o. 1 ed 3y			B-46 61:2606 677 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft. Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-		(FILL)	1.5		0.0 - 1.5	50	5-7-5	12			
2.5	675.0	CLAY, silty, brown, moderate plasticity, very stiff, dry to slightly moist, (CL), with trace black oxide nodules			1.5 - 3.0	22	5-6-6	12	14.7		
	672.5	CLAY, silty, orange brown, high plasticity, very stiff, moist, (CH), with trace black oxide nodules	3.5		4.0 - 5.5	100	7-7-9	16			
5.0		Boring Terminated	5.5		4.0 - 0.0	100	,-,-,	10			
7.5	<u>670.0</u>										
-	667.5										
10.0											
	665.0	Remarks: (a) Ground surface elevation									ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill I Grou	ation nt r Meth	nod	Tucker Station Roa Louisville, Xebec Rec S. Martin Rig Type Direct Push Hammer Typ Not encountered	<u>KY</u> Ilty 	eo-Pr	obe 7822 tomatic	DT	Boring Na Project N Elevation Started Complet Logged E Weather	o. ed			B-47 61:2606 677 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
			TOPSOIL, (2 inches) CLAY, silty, brown, moderate plasticity, soft, moist, (CL)			0.0 - 1.5	100	2-1-1	2			
2.5	675.0		CLAY, silty, brown to orange brown, high plasticity, stiff to very stiff, moist to very moist, (CH), with trace to little black oxide nodules			1.5 - 3.0	100	3-3-4	7	24.0		
5.0	672.5					4.0 - 5.5	100	5-6-7	13	32.1		
-	670.0		Boring Terminated	5.5		V						
7.5		-										
10.0	667.5	5										
	665.(-										



Loco Clier Drille Drill I	ition nt r Meth		Tucker Station Road Louisville, K Xebec Rea S. Martin Rig Type Direct Push Hammer Type Not encountered	(Y ty 	eo-Pr	obe 78221	 DT	Boring No Project N Elevation Started Complet Logged B Weather	o. ed			B-48 61:2606 676 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-	 675.0		TOPSOIL, (2 inches) CLAY, silty, brown, moderate plasticity, slightly moist, firm, (CL), with trace fine roots	<u>, 0.2</u> ,		0.0 - 1.5	67	1-2-2	4			
2.5	_		CLAY, silty, orange brown, high plasticity, stiff to very stiff, slightly moist to moist, (CH), with trace black oxide nodules.	2.2 _		1.5 - 3.0	100	4-4-5	9	23.0		
5.0	<u>672.</u> 					4.0 - 5.5	100	6-7-10	17			
		<u></u>	Boring Terminated	5.5								
7.5	667.5	5										
10.0	_	-										
	<u>665.(</u> 											



Locc Clier Drille Drill <i>N</i>	ition nt r Meth		Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	<u>Y</u> ty <u>Ge</u>	eo-Pr	obe 78221 omatic	 	Boring Na Project N Elevation Started Complet Logged E Weather	o. ed			B-49 61:2606 666 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-	 665.(TOPSOIL, (2 inches) CLAY, silty, brown, low plasticity, firm, slightly moist, (CL) CLAY, silty, orange brown, high plasticity, stiff to very stiff, moist to very moist, (CH)	0.2 0.4		0.0 - 1.5	93	2-2-3	5			
2.5						1.5 - 3.0	100	5-5-6	11	30.2		
5.0	<u>662.</u>					4.0 - 5.5	67	6-4-6	10			
	660.(Boring Terminated	5.5								
7.5	_	-										
	<u>657.</u> 	5										
10.0		- - 2										
			Remarks: (a) Ground surface elevatio					- +			<u> </u>	ept Plan Sheet 1 of 1



Proje Locc Clier Drille Drill M Grou	ition nt r ∧eth	od	Tucker Station Road Louisville, K' Xebec Realt S. Martin Rig Type Direct Push Hammer Type Not encountered	Y 	eo-Pr	obe 78221 omatic	 	Boring No Project N Elevation Started Complete Logged E Weather	o. ed			B-50 61:2606 662 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, (5 inches) CLAY, silty, red brown, high plasticity, stiff to hard, slightly moist to moist, (CH) with trace fine roots and black oxide nodules	0.4		0.0 - 1.5	100	2-4-3	7			
2.5	<u>660.0</u> 					1.5 - 3.0	100	4-4-6	10	19.6		
-	657.5											
5.0	_		Boring Terminated	5.5	Å	4.0 - 5.5	100	8-10-12	22			
7.5	 655.0	-) -										
		-										
10.0	<u>652.5</u> 	-										
	 650.0		Remarks: (a) Ground surface elevatior									ept Plan Sheet 1 of 1



Loca Clien Drille Drill N	Project Name Location Client Driller Drill Method Groundwater		Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type	Louisville, KY Xebec Realty S. Martin Rig Type Geo-Probe 7822DT								B-51 61:2606 673 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
	<u>672.5</u>		TOPSOIL, (3 inches) CLAY, silty, orange brown, high plasticity, stiff, slightly moist, (CH), with trace fine roots	0.3		0.0 - 1.5	94	2-3-5	8	20.7		
2.5	670.0		- with completely to highly weathered rock below approximately 2.7 feet	2.9		1.5 - 2.9	100	5-6-50/5"	50/5"			
		-	Boring Terminated at Direct Push Refusal									
5.0	667.5	5										
		-										
7.5	665.0											
10.0		-										
	662.5											
			Remarks: (a) Ground surface elevatio									ent Plan Sheet 1 of 1



									Boring No.			B-52				
	oject Name Tucker Station Road Property							Project N	61:2606							
Location Client			Louisville, K					Elevation	n	666 (a)						
			Xebec Real	ty				Started		10/22/2021						
Drille			<u>S. Martin</u> Rig Type	<u>be 78221</u>	Complet			10/22/2021								
Drill I			Direct Push Hammer Type	omatic	Logged By Weather				B. Emery 70's Partly Cloudy							
GIOU	maw	vater		Not encountered ATD												
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments				
 5.0	<u>6662.5</u>		TOPSOIL, (4 inches) CLAY, silty, brown, low plasticity, slightly moist, firm, (CL) - with completely to highly weathered rock below approximately 0.6 feet Boring Terminated at Direct Push Refusal	0.3		0.0 - 1.5	± 100 100	3-9-7 9-50/3"	Z 16 50/3"	20.9	UC					
 	<u>657.5</u>	-														



Loco Clier Drille Drill	Project Name Location Client Driller Drill Method Groundwater		Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type	Louisville, KY Xebec Realty S. Martin Rig Type Geo-Probe 7822DT								B-53 61:2606 670 (a) 10/22/2021 10/22/2021 B. Emery 70's Partly Cloudy
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
-			TOPSOIL, (6 inches) CLAY, silty, brown, low to high plasticity, slightly moist, (POSSIBLE FILL), with trace fine roots and few rock fragments	0.5		0.0 - 1.5	100	2-3-3	6	19.3		
	667.5					1.5 - 3.0	89	3-4-4	8	19.5		
-						4.0 - 5.5	28	3-3-3	6			
5.0	665.0	2	Boring Terminated	5.5								
7.5	662.5	5										
-		-										
10.0	<u>660.(</u>											
			Remarks: (a) Ground surface elevatio					-				ept Plan Sheet 1 of 1



Project Name Location Client Driller Drill Method Groundwater		Louisville, I Xebec Rea S. Martin Rig Type Direct Push	Louisville, KY Xebec Realty S. Martin Rig Type Geo-Probe 7822DT								B-54 61:2606 676 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy
Scale, ft.	0,	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
67: 67: 67: 67: 67: 67:		TOPSOIL, (3 inches) CLAY, silty, brown to tan brown, moderate plasticity, stiff, slightly moist to moist, (CL), with few black oxide nodules and trace organics - with completely to highly weathered rock below approximately 1.3 feet Boring Terminated at Direct Push Refusal	<u>0.3</u>		0.0 - 1.5	100	2-5-14	19	23.1		
	 7.5										
 663											



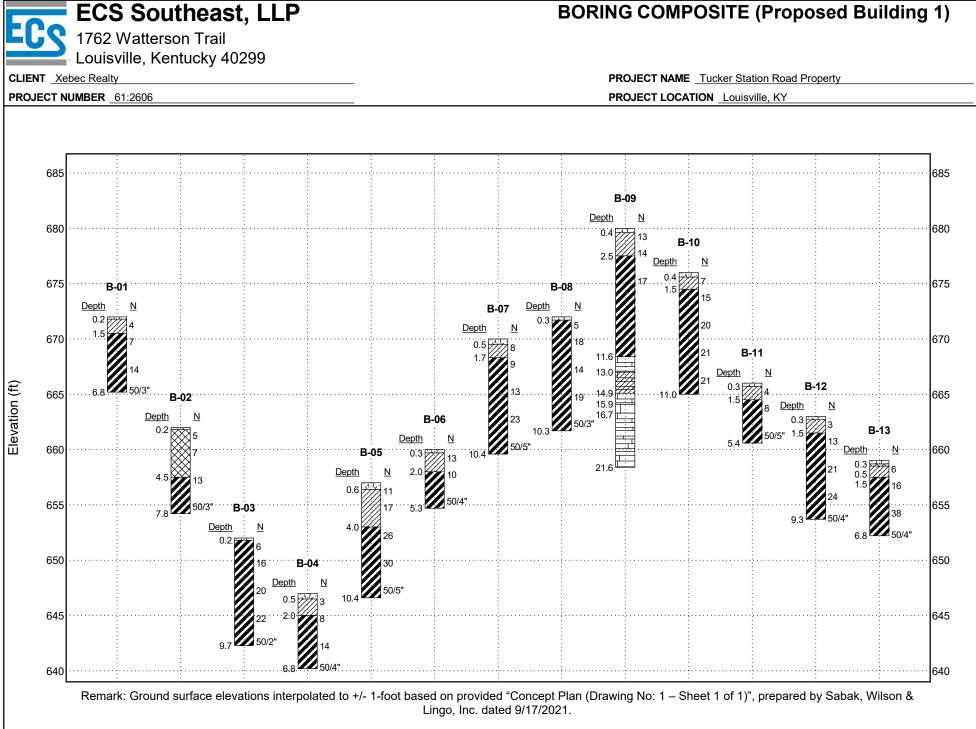
Project Name Location Client Driller Drill Method Groundwater		od	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	obe 78221 omatic	Boring No. Project No. Elevation Started Completed Logged By Weather		B-55 61:2606 670 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy					
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
			TOPSOIL, (4 inches) CLAY, silty, brown, moderate plasticity, firm, slightly moist to moist, (CL)	0.3		0.0 - 1.5	100	1-2-2	4			
2.5	 667.5					1.5 - 3.0	100	3-3-3	6	23.2		
5.0			CLAY, silty, brown, high plasticity, stiff, slightly moist, (CH), with few black oxide nodules - with completely to highly weathered rock below approximately 5 feet Boring Terminated at Direct Push	<u>3.8</u> 5.4		4.0 - 5.4	100	2-5-50/5"	50/5"	20.7		
7.5			Refusal									
		-										
<u>10.0</u>	<u>660.0</u> 											

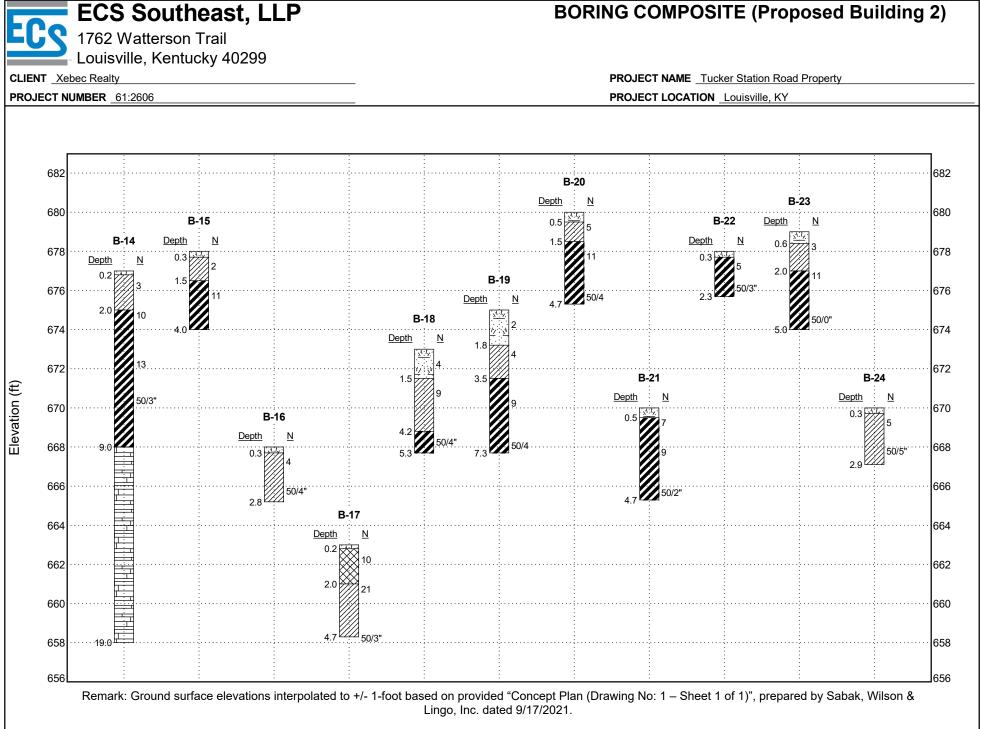


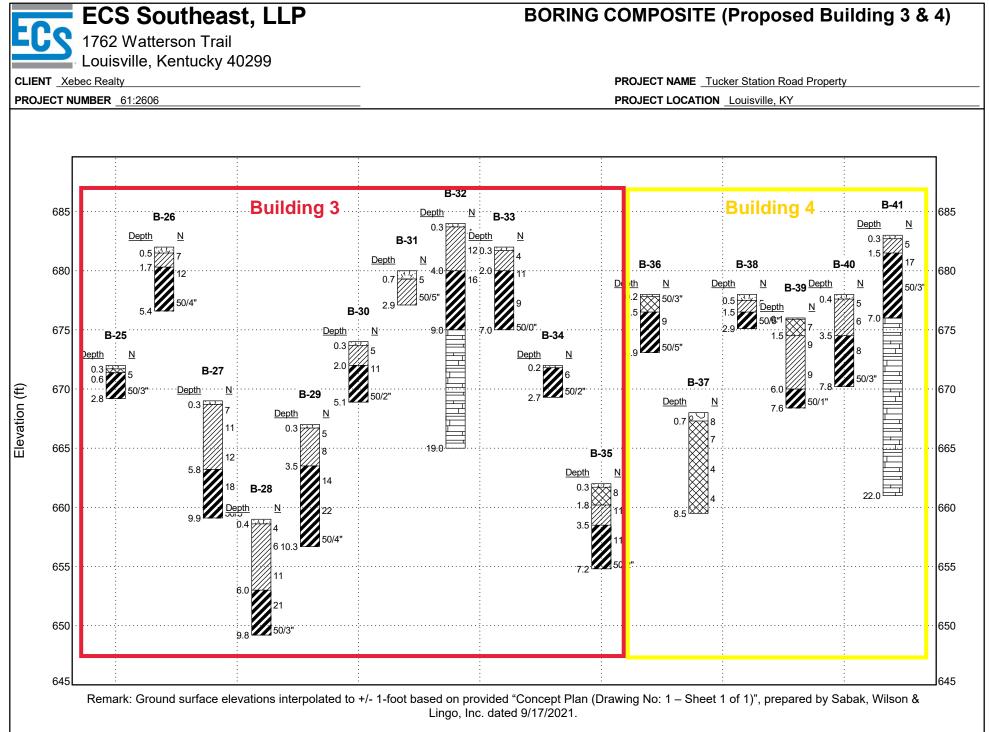
Project Name Location Client Driller Drill Method Groundwater		nod	Louisville, K Xebec Reali S. Martin Rig Type Direct Push Hammer Type	Louisville, KY Xebec Realty S. Martin Rig Type Geo-Probe 7822DT							B-56 61:2606 657 (a) 10/21/2021 10/21/2021 B. Emery 50's Partly Cloudy				
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments			
			TOPSOIL, (4 inches) CLAY, silty, tan brown, low plasticity, stiff, dry, (CL), with trace fine roots	0.3		0.0 - 1.5	94	3-4-4	8						
2.5	655.		CLAY, silty, orange brown with gray mottling, high plasticity, hard, dry to moist, (CH), with trace black oxide nodules	1.7		1.5 - 3.0	100	9-12-10	22	12.3					
	652.					4.0 - 5.5	94	8-8-9	17						
7.5	650.					6.5 - 8.0	100	10-10-10	20						
			Boring Terminated	8.0											
<u>10.0</u>	<u>647.</u> 645.	_													

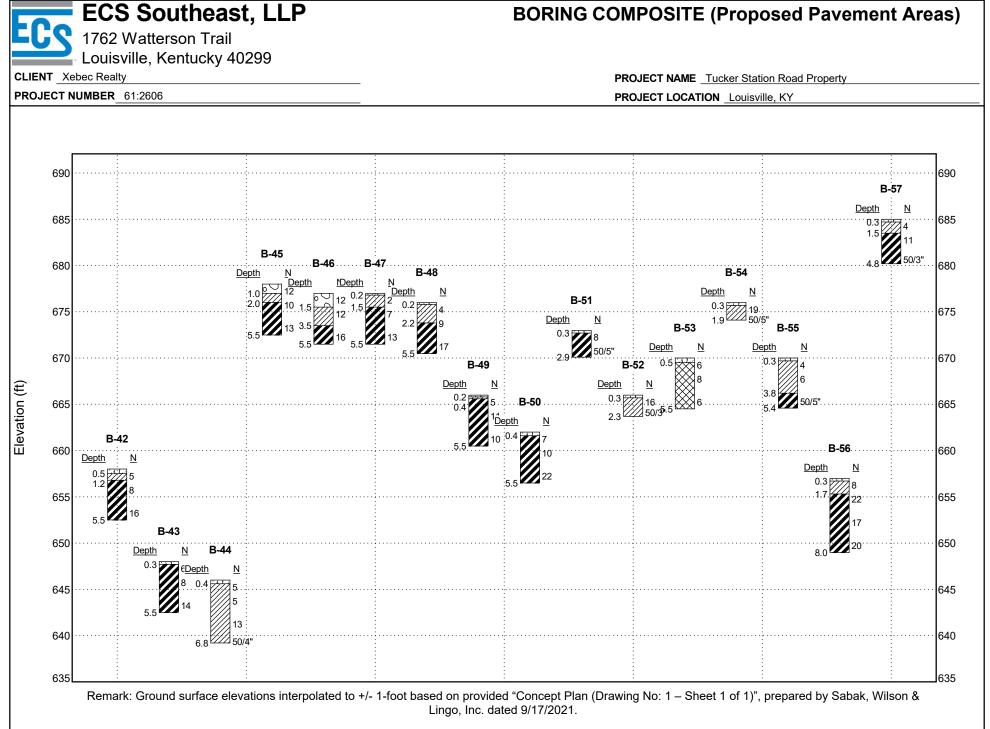


Project Name Location Client Driller Drill Method Groundwater		nod	Tucker Station Road Louisville, K Xebec Real S. Martin Rig Type Direct Push Hammer Type Not encountered	obe 78221	Boring No. Project No. Elevation Started Completed Logged By Weather		B-57 61:2606 685 (a) 10/21/2021 10/21/2021 B. Hasanzadeh 50's Partly Cloudy					
Scale, ft.	Elevation, ft.	Soil Symbol	Material Description and Classification	Depth, ft.	Sample Type	Sample Depth, ft.	Recovery, %	Standard Penetration Test Blows	N Value	Water Content, %	Uc, tsf	Comments
_			TOPSOIL, (3 inches) CLAY, silty, brown, low plasticity, firm, moist, (CL)	0.3		0.0 - 1.5	100	1-1-3	4	23.1		
2.5	682.		CLAY, silty, brown to orange brown with gray mottling, high plasticity, very stiff, moist to very moist, (CH), with trace black oxide nodules			1.5 - 3.0	100	6-6-5	11	30.8		
5.0	680.0		- with completely to highly weathered rock below approximately 4.5 feet Boring Terminated at Direct Push	4.8		4.0 - 4.8	100	9-50/3"	50/3"			
-		_	Refusal									
7.5	677.	5										
<u>10.0</u>	<u>6/5.</u> 											









Field Procedures

General

ECS conducts field sampling and testing procedures in general accordance with methods of the American Society for Testing Materials (ASTM) and widely accepted geotechnical engineering standards. A brief description of the procedures we utilize is provided in the following paragraphs.

Soil Borings (ASTM D-1452)

Soil borings are made with hollow stem augers or continuous augers which are mechanically advanced by a powered drill rig. At selected depths, soil samples are obtained with either a splitbarrel sampler or a thin wall tube sampler. Soil borings are advanced to refusal, or to maximum depths as defined in our scope of work. The boring data, including sampling intervals, penetration resistances, soil classifications, and groundwater observations, are presented on the attached Boring Records.

Boring Locations and Elevations

Boring locations typically are selected by our project manager. The project manager establishes the boring locations in the field by pacing or measuring distances and estimating angles relative to existing site landmarks. When topographic plans of the site are provided, the project manager estimates the surface elevation of the boring locations using available information. Surveying to determine the locations and elevations of the borings is beyond the scope of typical geotechnical studies; therefore, the boring locations and elevations should be considered approximate.

Standard Penetration Test (SPT) Split-Barrel Samples (ASTM D-1586)

A split-barrel or "splitspoon" is inserted into the borehole to obtain soil samples. The sampler is driven three, 6-inch increments with a 140-pound hammer falling from a height of 30 inches. The "standard penetration resistance" or "N-value" is the number of hammer blows required to drive the sampler the final 12 inches. The N-value, when properly evaluated, is an index of soil strength and/or density. Upon completion of each standard penetration test, the sampler is brought to the surface and the tube is opened to expose the recovered soil. Our project manager examines the sample, records the soil description and other pertinent information, and places a representative portion of the soil into a sealed container for transportation to our laboratory.

Rock Coring (ASTM D-2113)

A diamond studded bit, fastened to the end of a hollow double tube core barrel, is rotated at sufficient speeds to penetrate the refusal material. At the completion of each core run (limited by the length of core barrel, typically 5 or 10 feet), the core barrel is returned to the surface and the materials contained within the swivel mounted inner tube are removed. The materials recovered are placed in a sample box, visually classified, and the core depth, recovery, and Rock Quality Designation (RQD), are determined. The recovery is the percentage of recovered core with respect to the total length cored. The RQD is the percentage of the core revered in hard, sound and naturally unbroken pieces 4 inches or greater in length. The recovery and RQD are related to the soundness and continuity of the refusal material.

Water Level Readings

Water level readings are taken in each borehole upon the completion of drilling or excavation. In low permeability soils, such as silts and clays, the water level in the boreholes may take many hours to stabilize. Groundwater levels may be dependent upon recent rainfall activity and other site specific factors. Since these conditions may change with time, the water level information presented on the Boring Records represents the conditions only at the time each measurement was taken.

Boring Records

Our interpretation of the conditions encountered at each location is indicated on the Boring Records, which are prepared from the observations of the ECS field engineer or geologist during drilling or excavation, our engineering review of the soil samples obtained, the results of laboratory testing on selected samples, and our experience with similar subsurface conditions. Soil descriptions are made using the Unified Soil Classification System and/or ASTM D-2488 as guides. The depths designating strata changes are estimations and only representative of depths at that specific boring location. In many geologic settings, the transition between strata is gradual. A Boring Legend, which defines the symbols and other pertinent information presented on the Boring Records, is provided with this report. The subsurface conditions indicated on our Boring Records represent only the conditions encountered at the specific boring location at the time of our exploration. The groundwater observations were made at the time of drilling and may vary with changes in the season and weather.

Refusal

Refusal is the term applied to material that cannot be penetrated with augers or has a standard penetration resistance exceeding 50 blows per 6-inch increment. Refusal may be encountered on continuous bedrock, discontinuous floaters, cemented soil, weathered rock, debris, buried structures, or other hard subsurface materials. Refusal materials can be evaluated only by obtaining a core of the material. This limitation must be considered when evaluating refusal depths where coring is not conducted.

Laboratory Procedures

General

Laboratory tests are generally conducted to satisfy one or more of the following objectives: (1) confirmation of visual-manual soil identification; (2) determination of index values used to estimate soil engineering properties (i.e., strength, compressibility and permeability); or (3) direct measurement of specific soil properties. The tests selected for a given project are dependent on the subsurface conditions encountered, as well as specific project requirements, such as structural loads and planned grade changes. The results of laboratory tests conducted for this project are listed on the Boring Records, Laboratory Test Data Summary, or laboratory data curves in the Appendix. Brief descriptions of the test procedures are provided below.

Description and Identification of Soils (Visual-Manual Procedure) (ASTM D 2488)

The Visual-Manual Procedure provides a general guide to the engineering properties of soils and enables the engineer to apply past experience to current situations. Samples obtained during the field exploration are examined and visually described and identified by a geotechnical engineer or geologist. The soils are typically identified according to predominant particle size (clay, silt, sand, etc.), consistency (based on apparent stiffness and the number of blows from standard penetration tests), color, moisture and group symbol (CL, CH, SP, SC, etc.). Unless otherwise indicated, the soil descriptions in this report are based on the Visual-Manual Procedure.

Classification of Soils for Engineering Purposes (Unified Soil Classification System) (ASTM D 2487)

The Visual-Manual Procedure described above is primarily qualitative. The Unified Soil Classification System (USCS) is used when precise soil classification is required. The USCS is based on laboratory determination of particle-size characteristics, liquid limit, and plasticity index. Using these test results, the soil can be classified according to the Unified Classification System, which provides an index for estimating soil behavior.

Water (Moisture) Content of Soil (ASTM D 2216)

Moisture content is one of the most important index properties used in establishing a correlation between soil behavior and soil properties such as strength and compressibility. The moisture content, along with the liquid and plastic limits, are used to express the relative consistency or liquidity index of a soil. Increasing moisture contents typically reflect lower strengths for a given soil. The soil moisture content is the ratio, expressed as a percentage, of the mass of "pore" or "free" water in a given mass of soil to the mass of the solid soil. Moisture content samples are taken from the sealed container obtained during the field exploration phase of a project. Each sample is weighed, and then placed in an oven set to $110^{\circ}C + 5^{\circ}$. Each sample remains in the oven until the free moisture evaporates. Each dried sample is removed from the oven, allowed to cool, and then weighed. The moisture content is computed by dividing the weight of evaporated water by the weight of the dry sample.

Liquid Limit, Plastic Limit, and Plasticity Index of Soils (ASTM D 4318)

Depending upon the relative moisture content, a fine-grained soil may occur in a liquid, plastic, or solid state. In current usage, the liquid limit (LL) and plastic limit (PL) of a soil are referred to as the "Atterberg Limits", which establish the approximate moisture contents at which the soil changes state. This test method is an integral part of several engineering classification systems to characterize the fine grained fractions of soils. It is also used with other soil properties to correlate with engineering behavior such as compressibility, permeability, compactability, shrink-swell, and shear strength. The liquid limit is the moisture content at which a soil becomes sufficiently "wet" to behave as a heavy viscous fluid (i.e., transition from plastic to liquid state). It is defined as the moisture content at which the soil, when placed in a standard brass bowl, makes a 1/2-inch closure

in a groove cut through the soil after the bowl is dropped 25 times at a specified height and rate. The plastic limit is the moisture content at which the soil begins to lose its plasticity (i.e., transition from plastic to semi-solid state). It is defined as the lowest moisture content at which the soil can be rolled into 1/8-inch diameter threads without crumbling. The plasticity index (PI) is the difference between the liquid limit and the plastic limit, and is the range of moisture content over which a soil deforms as a plastic material.

Important Information about This Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

The Geoprofessional Business Association (GBA) has prepared this advisory to help you - assumedly a client representative - interpret and apply this geotechnical-engineering report as effectively as possible. In that way, clients can benefit from a lowered exposure to the subsurface problems that, for decades, have been a principal cause of construction delays, cost overruns, claims, and disputes. If you have questions or want more information about any of the issues discussed below, contact your GBA-member geotechnical engineer. Active involvement in the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project.

Geotechnical-Engineering Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a given civil engineer will not likely meet the needs of a civilworks constructor or even a different civil engineer. Because each geotechnical-engineering study is unique, each geotechnicalengineering report is unique, prepared *solely* for the client. *Those who rely on a geotechnical-engineering report prepared for a different client can be seriously misled*. No one except authorized client representatives should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one – not even you – should apply this report for any purpose or project except the one originally contemplated*.

Read this Report in Full

Costly problems have occurred because those relying on a geotechnicalengineering report did not read it *in its entirety*. Do not rely on an executive summary. Do not read selected elements only. *Read this report in full*.

You Need to Inform Your Geotechnical Engineer about Change

Your geotechnical engineer considered unique, project-specific factors when designing the study behind this report and developing the confirmation-dependent recommendations the report conveys. A few typical factors include:

- the client's goals, objectives, budget, schedule, and risk-management preferences;
- the general nature of the structure involved, its size, configuration, and performance criteria;
- the structure's location and orientation on the site; and
- other planned or existing site improvements, such as retaining walls, access roads, parking lots, and underground utilities.

Typical changes that could erode the reliability of this report include those that affect:

- the site's size or shape;
- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light-industrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes – even minor ones – and request an assessment of their impact. *The geotechnical engineer who prepared this report cannot accept responsibility or liability for problems that arise because the geotechnical engineer was not informed about developments the engineer otherwise would have considered.*

This Report May Not Be Reliable

Do not rely on this report if your geotechnical engineer prepared it:

- for a different client;
- for a different project;
- for a different site (that may or may not include all or a portion of the original site); or
- before important events occurred at the site or adjacent to it; e.g., man-made events like construction or environmental remediation, or natural events like floods, droughts, earthquakes, or groundwater fluctuations.

Note, too, that it could be unwise to rely on a geotechnical-engineering report whose reliability may have been affected by the passage of time, because of factors like changed subsurface conditions; new or modified codes, standards, or regulations; or new techniques or tools. *If your geotechnical engineer has not indicated an "apply-by" date on the report, ask what it should be*, and, in general, *if you are the least bit uncertain* about the continued reliability of this report, contact your geotechnical engineer before applying it. A minor amount of additional testing or analysis – if any is required at all – could prevent major problems.

Most of the "Findings" Related in This Report Are Professional Opinions

Before construction begins, geotechnical engineers explore a site's subsurface through various sampling and testing procedures. *Geotechnical engineers can observe actual subsurface conditions only at those specific locations where sampling and testing were performed.* The data derived from that sampling and testing were reviewed by your geotechnical engineer, who then applied professional judgment to form opinions about subsurface conditions throughout the site. Actual sitewide-subsurface conditions may differ – maybe significantly – from those indicated in this report. Confront that risk by retaining your geotechnical engineer to serve on the design team from project start to project finish, so the individual can provide informed guidance quickly, whenever needed.

This Report's Recommendations Are Confirmation-Dependent

The recommendations included in this report – including any options or alternatives – are confirmation-dependent. In other words, *they are not final*, because the geotechnical engineer who developed them relied heavily on judgment and opinion to do so. Your geotechnical engineer can finalize the recommendations *only after observing actual subsurface conditions* revealed during construction. If through observation your geotechnical engineer confirms that the conditions assumed to exist actually do exist, the recommendations can be relied upon, assuming no other changes have occurred. *The geotechnical engineer who prepared this report cannot assume responsibility or liability for confirmationdependent recommendations if you fail to retain that engineer to perform construction observation*.

This Report Could Be Misinterpreted

Other design professionals' misinterpretation of geotechnicalengineering reports has resulted in costly problems. Confront that risk by having your geotechnical engineer serve as a full-time member of the design team, to:

- confer with other design-team members,
- help develop specifications,
- review pertinent elements of other design professionals' plans and specifications, and
- be on hand quickly whenever geotechnical-engineering guidance is needed.

You should also confront the risk of constructors misinterpreting this report. Do so by retaining your geotechnical engineer to participate in prebid and preconstruction conferences and to perform construction observation.

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can shift unanticipated-subsurface-conditions liability to constructors by limiting the information they provide for bid preparation. To help prevent the costly, contentious problems this practice has caused, include the complete geotechnical-engineering report, along with any attachments or appendices, with your contract documents, *but be certain to note conspicuously that you've included the material for informational purposes only*. To avoid misunderstanding, you may also want to note that "informational purposes" means constructors have no right to rely on the interpretations, opinions, conclusions, or recommendations in the report, but they may rely on the factual data relative to the specific times, locations, and depths/elevations referenced. Be certain that constructors know they may learn about specific project requirements, including options selected from the report, *only* from the design drawings and specifications. Remind constructors that they may perform their own studies if they want to, and *be sure to allow enough time* to permit them to do so. Only then might you be in a position to give constructors the information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions. Conducting prebid and preconstruction conferences can also be valuable in this respect.

Read Responsibility Provisions Closely

Some client representatives, design professionals, and constructors do not realize that geotechnical engineering is far less exact than other engineering disciplines. That lack of understanding has nurtured unrealistic expectations that have resulted in disappointments, delays, cost overruns, claims, and disputes. To confront that risk, geotechnical engineers commonly include explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely*. Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The personnel, equipment, and techniques used to perform an environmental study – e.g., a "phase-one" or "phase-two" environmental site assessment – differ significantly from those used to perform a geotechnical-engineering study. For that reason, a geotechnicalengineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated subsurface environmental problems have led to project failures*. If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. As a general rule, *do not rely on an environmental report prepared for a different client, site, or project, or that is more than six months old.*

Obtain Professional Assistance to Deal with Moisture Infiltration and Mold

While your geotechnical engineer may have addressed groundwater, water infiltration, or similar issues in this report, none of the engineer's services were designed, conducted, or intended to prevent uncontrolled migration of moisture – including water vapor – from the soil through building slabs and walls and into the building interior, where it can cause mold growth and material-performance deficiencies. Accordingly, *proper implementation of the geotechnical engineer's recommendations will not of itself be sufficient to prevent moisture infiltration*. Confront the risk of moisture infiltration by including building-envelope or mold specialists on the design team. *Geotechnical engineers are not buildingenvelope or mold specialists*.



Telephone: 301/565-2733 e-mail: info@geoprofessional.org www.geoprofessional.org

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